

Design Example Report

| | |
|------------------------|---|
| Title | <i>50 W 2-Stage Boost and Isolated Flyback LED Ballast Using HiperPFS™-4 PFS7623C and LYTSwitch™-6 LYT6067C with Power and CCT Selection</i> |
| Specification | 100 VAC – 277 VAC Input; 30 V – 42 V, 1200 mA Output |
| Application | LED Lighting Ballast |
| Author | Applications Engineering Department |
| Document Number | DER-847 |
| Date | January 16, 2020 |
| Revision | 1.0 |

Summary and Features

- With integrated PFC function, PF >0.90
- Low THD <15% at nominal
- Accurate output voltage and current regulation, ±5%
- Low ripple current
- Highly energy efficient, >89% at 230 VAC
- Low cost and low component count for compact PCB solution
- Compatible with 3-Way dimming application
- With Multi-Set Feature: Power Selection and CCT Selection
- Integrated protection and reliability features
 - Output short-circuit
 - Line and output OVP
 - Line surge or line overvoltage
 - Thermal foldback and over temperature shutdown with hysteretic automatic power recovery
- No damage during line brown-out or brown-in conditions
- Meets IEC 2.5 kV ring wave, 1 kV differential surge
- Meets EN55015 conducted EMI

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PATENT INFORMATION

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Important Note: Although this board is designed to satisfy safety isolation requirements, the engineering prototype has not been agency approved. Therefore, all testing should be performed using an isolation transformer to provide the AC input to the prototype board.



1 Introduction

This engineering report describes a constant voltage (CV) and constant current (CC) output 42 W LED ballast with 3-way dimming function, Correlated Color Temperature (CCT) function, and power selection multi-set feature. At constant voltage application, the LED ballast is designed to provide a 42 V output voltage across 0 mA to 1200 mA output current load while at constant current mode operation, it can provide 1200 mA (3-way dimmable) constant current at 42 V – 30 V LED voltage string. The design is optimized to operate from an input voltage range of 100 VAC to 277 VAC.

The LED ballast employs a two-stage design with a boost PFC at first stage and an isolated flyback DC-DC for the secondary stage. The boost PFC utilizes HiperPFS-4 device while the second stage flyback uses LYTSwitch-6 controller.

The HiperPFS-4 devices incorporate a continuous conduction mode (CCM) boost PFC controller, gate driver and 600 V power MOSFET in a single power package. This device eliminates the need for external current sense resistors and their associated power loss, and use an innovative control technique that adjusts the switching frequency over output load, input line voltage, and input line cycle.

LYTSwitch-6 ICs simplifies the flyback stage by combining primary, secondary and feedback circuits in a single surface IC. This IC includes an innovative new technology, FluxLink™, which safely bridges the isolation barrier and eliminates the need for an optocoupler. The single architecture of LYTSwitch-6 allows the IC to have primary and secondary controllers, with sense elements and a safety-rated mechanism into a single IC.

DER-847 key design goals offer high power factor (>0.90), low THD (<15%) at nominal input, high efficiency, and low component count at universal input voltages.

The document contains the power supply specification, schematic, bill of materials, transformer documentation, printed circuit layout, and performance data.



Figure 1 – Populated Circuit Board.

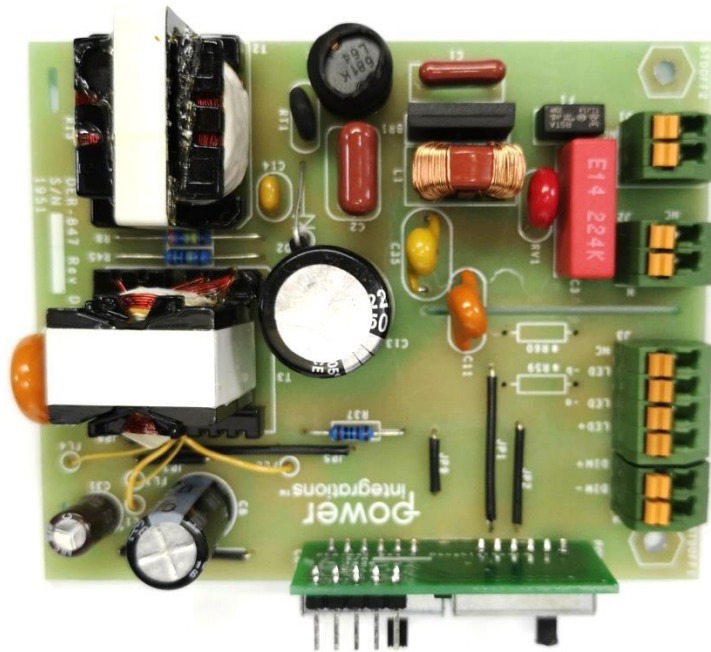


Figure 2 – Populated Circuit Board, Top View.

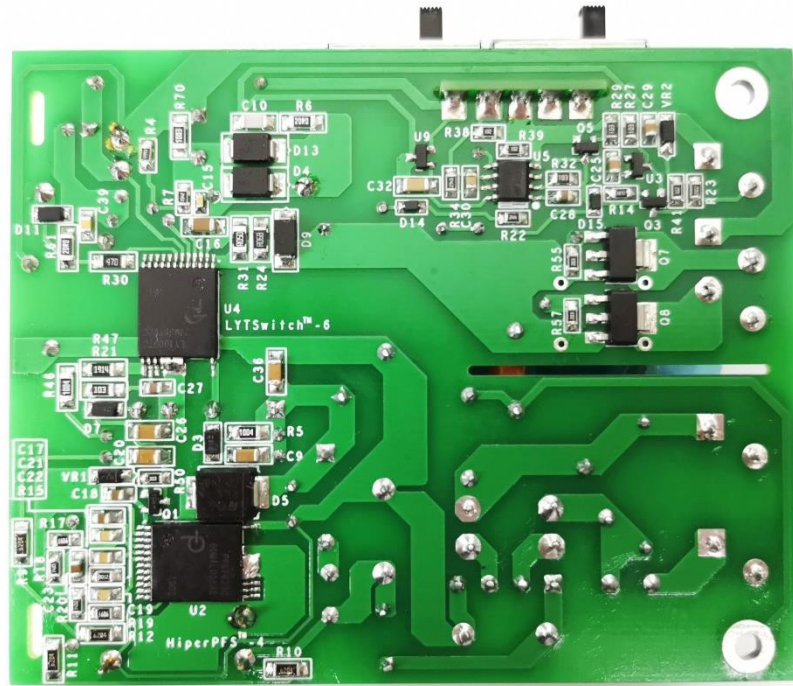


Figure 3 – Populated Circuit Board, Bottom View.

2 Power Supply Specification

The table below represents the minimum acceptable performance of the design. Actual performance is listed in the results section.

| Description | Symbol | Min | Typ | Max | Units | Comment | |
|---------------------------|------------|----------------------|------|------|-------|---|--|
| Input | | | | | | | |
| Voltage | V_{IN} | 100 | 230 | 277 | VAC | 2-Wire Floating Output or 3-Wire with P.E. | |
| Frequency | f_{LINE} | | 50 | | Hz | | |
| Output | | | | | | | |
| Output Voltage | V_{OUT} | 30 | 36 | 42 | V | ±5% | |
| Output Current | I_{OUT} | 1150 | 1200 | 1250 | mA | | |
| Total Output Power | | | | | | | |
| Continuous Output Power | P_{OUT} | | 50 | | W | | |
| Efficiency | | | | | | | |
| Full Load | η | | 89 | | % | 230 V / 50 Hz at 25 °C. | |
| Environmental | | | | | | | |
| Conducted EMI | | CISPR 15B / EN55015B | | | | | |
| Safety | | Isolated | | | | | |
| Ring Wave (100 kHz) | | | 2.5 | | kV | | |
| Differential Mode (L1-L2) | | | 1.0 | | kV | Surge Rating. | |
| Power Factor | | | 0.9 | | | Measured at 230 VAC / 50 Hz. | |
| Ambient Temperature | T_{AMB} | | | 50 | °C | Free Air Convection, Sea Level. | |

3 Schematic Diagram

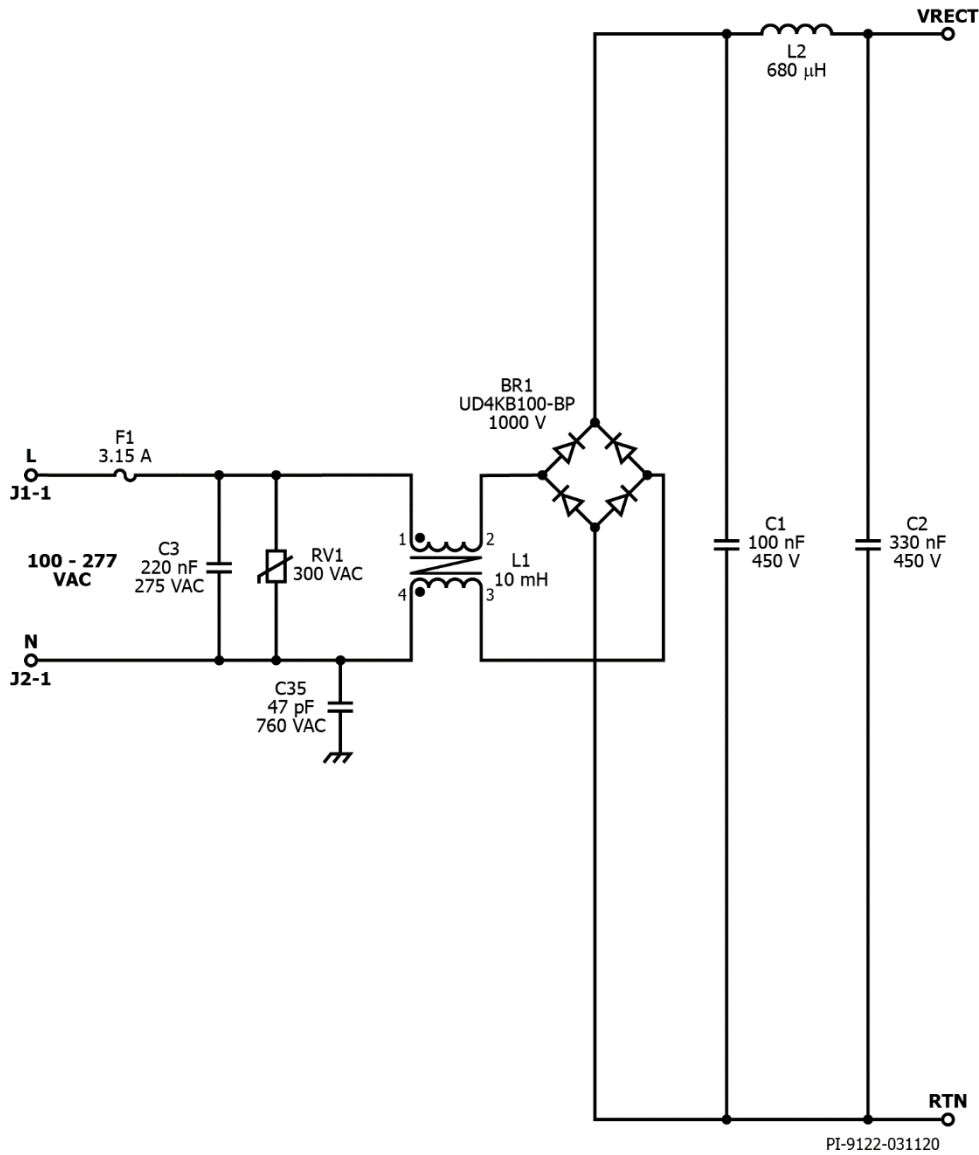


Figure 4 – Schematic of the Input Section.

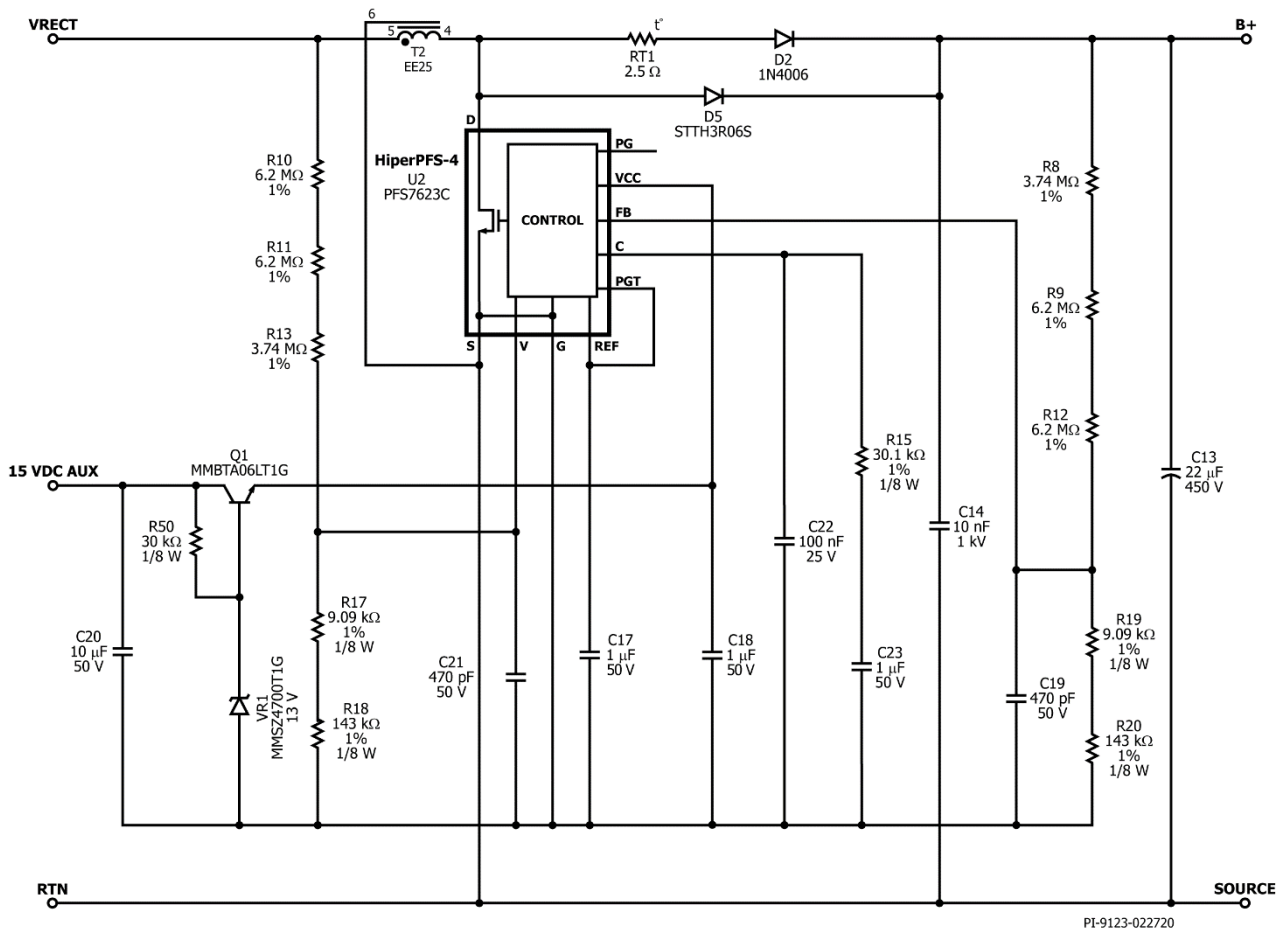


Figure 5 – Schematic of the PFC Section.

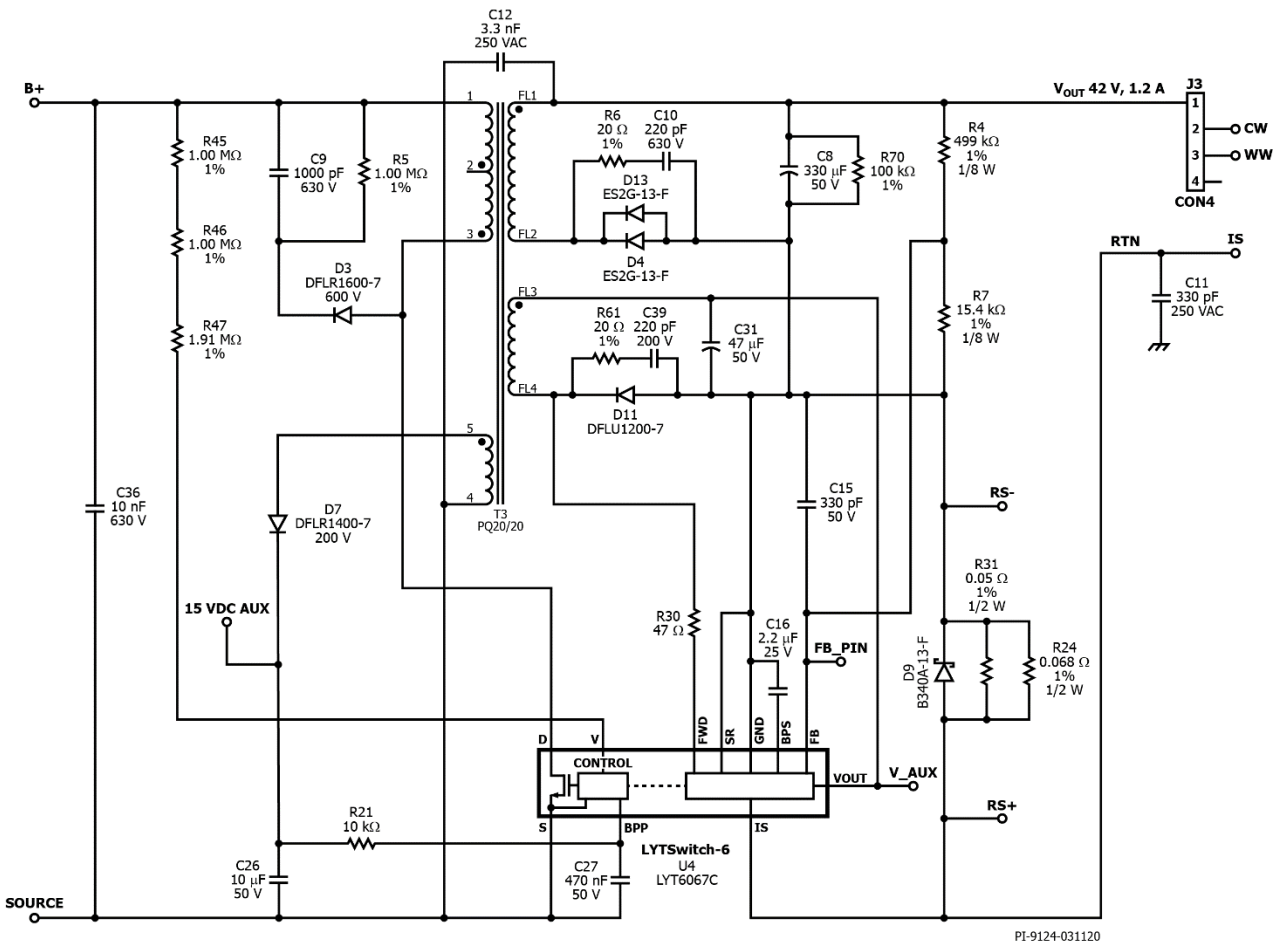


Figure 6 – Schematic of the Power Section.



4 Circuit Description

A two-stage LED ballast circuit is designed with power and CCT selection features, and 3-way dimming function. The first stage is a boost PFC using PFS7623C from the HiperPFS-4 family of devices. The second stage is an isolated flyback DC-DC power supply using a LYTSwitch-6 IC.

HiperPFS-4 PFS7623C is a PFC controller with an integrated power MOSFET and external boost diode. This stage is intended as a general purpose platform that operates from 100 VAC to 277 VAC input voltage that provides a highly efficient single-stage power factor corrector regulated at 410 V DC output voltage and continuous output power of 54 W.

LYTSwitch-6 ICs incorporate the primary FET, the primary-side controller and a secondary-side synchronous rectification controller. This ICs also include an innovative new technology, FluxLink™, which safely bridges the isolation barrier and eliminates the need for an optocoupler.

4.1 *Input EMI Filter and Rectifier*

The input fuse F1 provides safety protection. Varistor RV1 acts as a voltage clamp that limits the voltage spike on the primary during line transient voltage surge events. A 300 V rated part was selected, being above the maximum specified operating input voltage (277 V). The AC input voltage is full-wave rectified by BR1 to achieve good power factor and low THD. Capacitors C1, C2 and L2 form a pi filter which together with C3 suppresses differential mode noise. Common mode noise is suppressed by common mode choke L1 together with Y capacitor C35. Additional Y capacitor C11 was added for earth wire connection to suppress common mode noise.

4.2 **First Stage: Boost PFC Using HiperPFS-4**

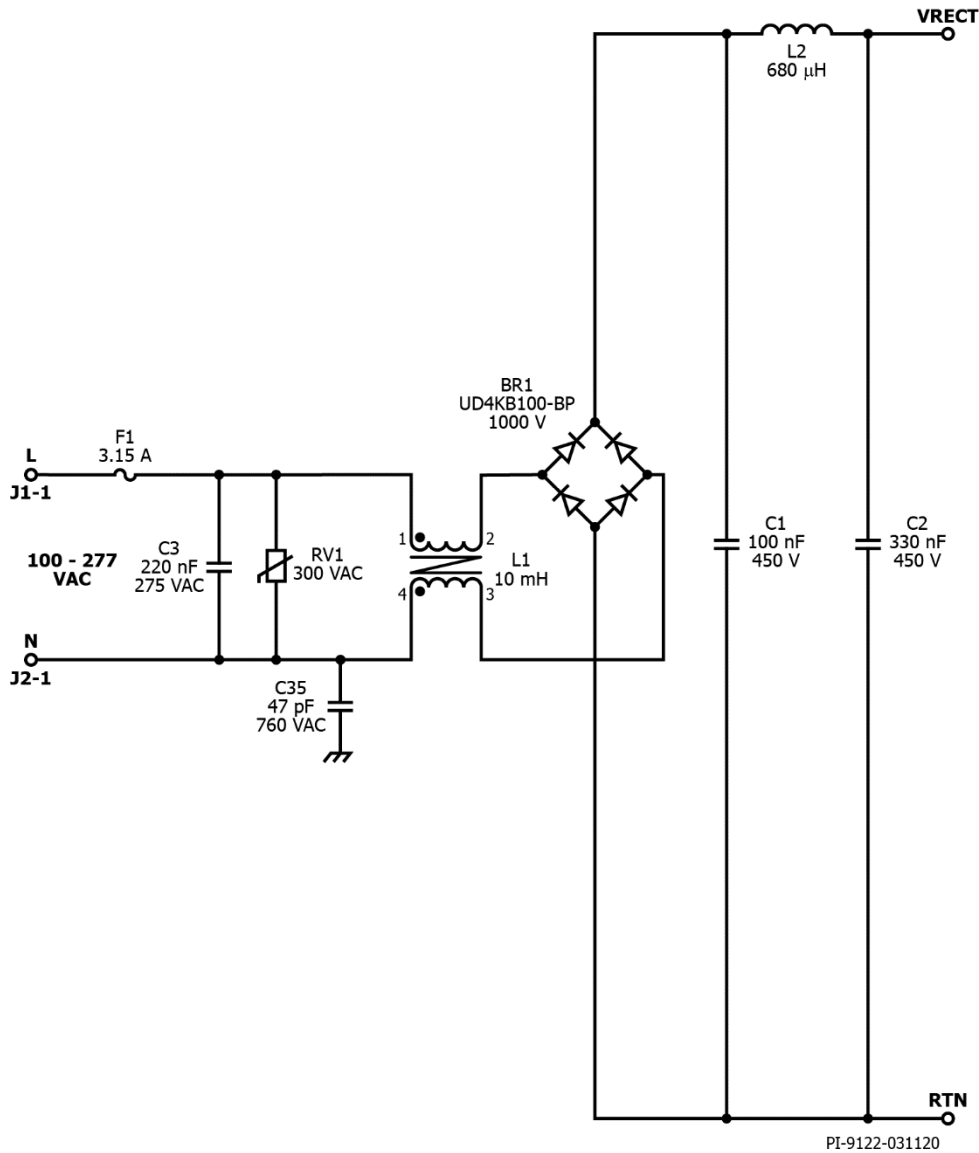


Figure 7 – Schematic of the Input Section.



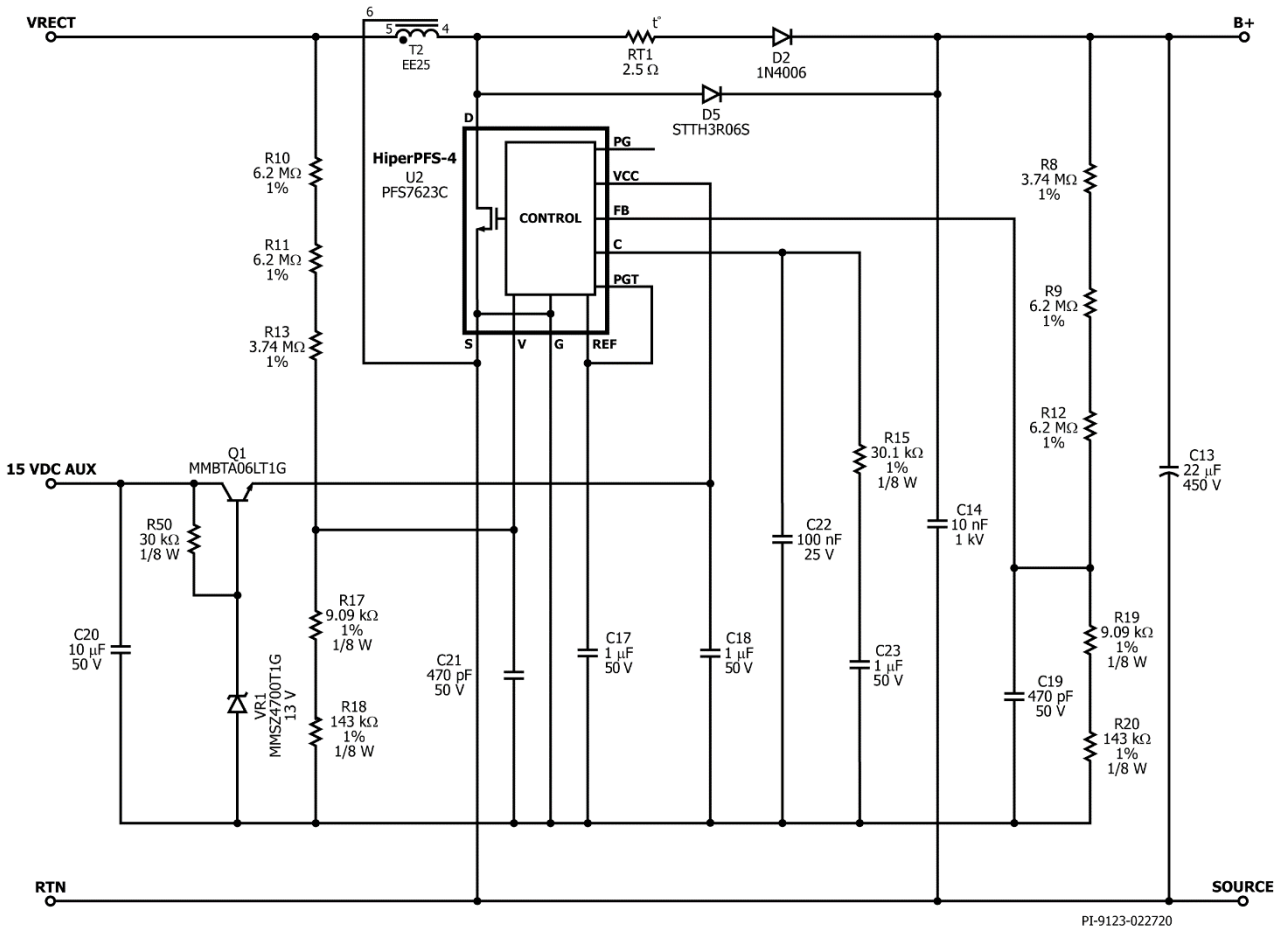


Figure 8 – Schematic of the PFC Section.

The boost converter stage consists of the boost inductor T2 and the HiperPFS-4 PFS7623C IC U2. This converter stage operates as a PFC boost converter, thereby maintaining a sinusoidal input current to the power supply while regulating a DC output voltage. On the other hand, boost diode D5 is an STTH3R06S for cost-effective solution with balanced EMI and switching speed performance.

Diode D2 and NTC resistor RT1 provide an initial path for the inrush current at start up. This is important as a way to bypass the switching inductor T2 and switch U2 in order to prevent a resonant interaction between the boost inductor and output bulk capacitor C13. The IC is then powered on the VCC pin by an external bias from the T3. This external bias provides 20 V DC, which is then regulated by C20, Q1, R50 and VR1 to around 12 V DC.

Capacitor C14 provides a short, high-frequency return path to RTN. This effectively improves EMI results and reduces U2 MOSFET drain voltage overshoot during turn off. Capacitor C17 is used to select the power mode of the IC. 1 μF was used for full power



mode. Capacitor C22, C23 and resistor R15 used for the loop compensation network are required to tailor the loop response to ensure low cross-over frequency and sufficient phase margin. Its recommended values are 100 nF, 1 μ F and 30.1 k Ω respectively.

Resistor R8, R9, R12, R19 and R20 form the resistor network for the feedback. Voltage at feedback must be typically at 3.85 V with 3.82 V at its minimum. Capacitor C19 attenuates high frequency noise.

Resistor R10, R11, R13, R17 and R18 comprise the functionality for the VOLTAGE MONITOR (V) pin. Capacitor C21 filters noise coupled into the V pin. This minimizes power dissipation and standby power consumption. This also features brown-in/out detection thresholds and incorporates a weak current source that acts as a pull-down in the event of an open circuit condition.

4.3 Second Stage: Isolated Flyback DC-DC Using LYTSwitch-6

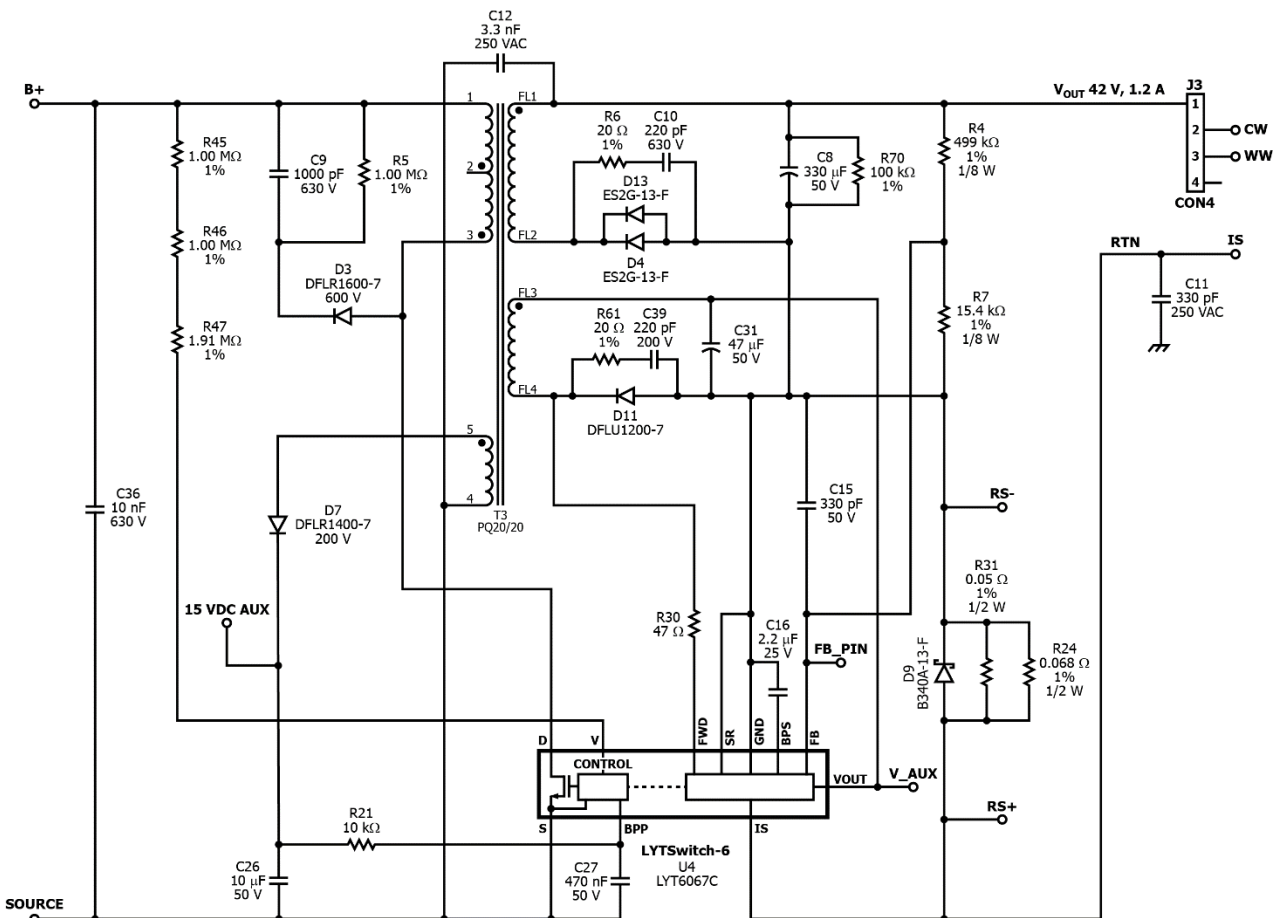


Figure 9 – Isolated Flyback DC-DC Schematic.



The second stage circuit topology is a flyback DC-DC power supply controlled by the LYTSwitch-6 IC. One side of the transformer (T3) primary is connected to the positive output terminal of the PFC while the other side is connected to the integrated 650 V power MOSFET inside the LYTSwitch-6 IC (U4). A low cost RCD clamp formed by D3, R5 and C9 limits the peak Drain voltage spike across U4 at the instant turn-off of the MOSFET. The clamp helps dissipate the energy stored in the leakage reactance of transformer T3.

The VOLTAGE MONITOR (V) pin of the LYTSwitch-6 IC is connected to the positive of the bulk capacitor (C13) via V pin resistors R45, R46, and R47 to provide input voltage information. The voltage across the bulk capacitor (C13) is sensed and converted into current through R45, R46 and R47 to provide detection of overvoltage. These resistors detect an overvoltage of 441 V which is between the DC output of the 1st stage (410 V) and the bulk capacitor rating (450 V). The I_{OV} determines the input overvoltage threshold.

The IC is kick-started by an internal high-voltage current source that charges the BPP pin capacitor C27 when AC is first applied. The primary-side will listen for secondary request signals for around 82ms. After initial power-up, primary-side assumes control first and requires a handshake to pass the control to the secondary-side. During normal operation, the primary-side block is powered from an auxiliary winding on the transformer. The output of this winding is rectified and filtered using diode D7 and capacitor C26. Resistor R21 limits the current being supplied to the BPP pin of the LYTSwitch-6 (U4). This auxiliary winding also powers the PFS7623C in the first stage.

The secondary side control of the LYTSwitch-6 IC provides output voltage, output current sensing. The secondary winding of the transformer is rectified by D4 and D13 and filtered by the output capacitor C8. Adding an RC snubber (R6 and C10) across the output diodes reduces voltage stress across them.

The secondary-side of the IC is powered from an auxiliary winding FL3 and FL4. During constant voltage mode operation, output voltage regulation is achieved by sensing the output voltage via divider resistors R4 and R7. The voltage across R7 is fed into the FB pin with an internal reference voltage threshold of 1.265 V. Filter capacitor C15 is added across R7 to eliminate unwanted noise. This noise might trigger the OVP function or might increase the output ripple voltage.

During constant current operation, the output current is set by the sense resistors R31 and R24 across the IS pin and the GND pin. The internal reference threshold for the IS pin is 35.9 mV. Diode D9 in parallel with the current sense resistor serves as protection during output short-circuit conditions.

4.4 **3-in-1 Dimming, CCT, and Power Selection**

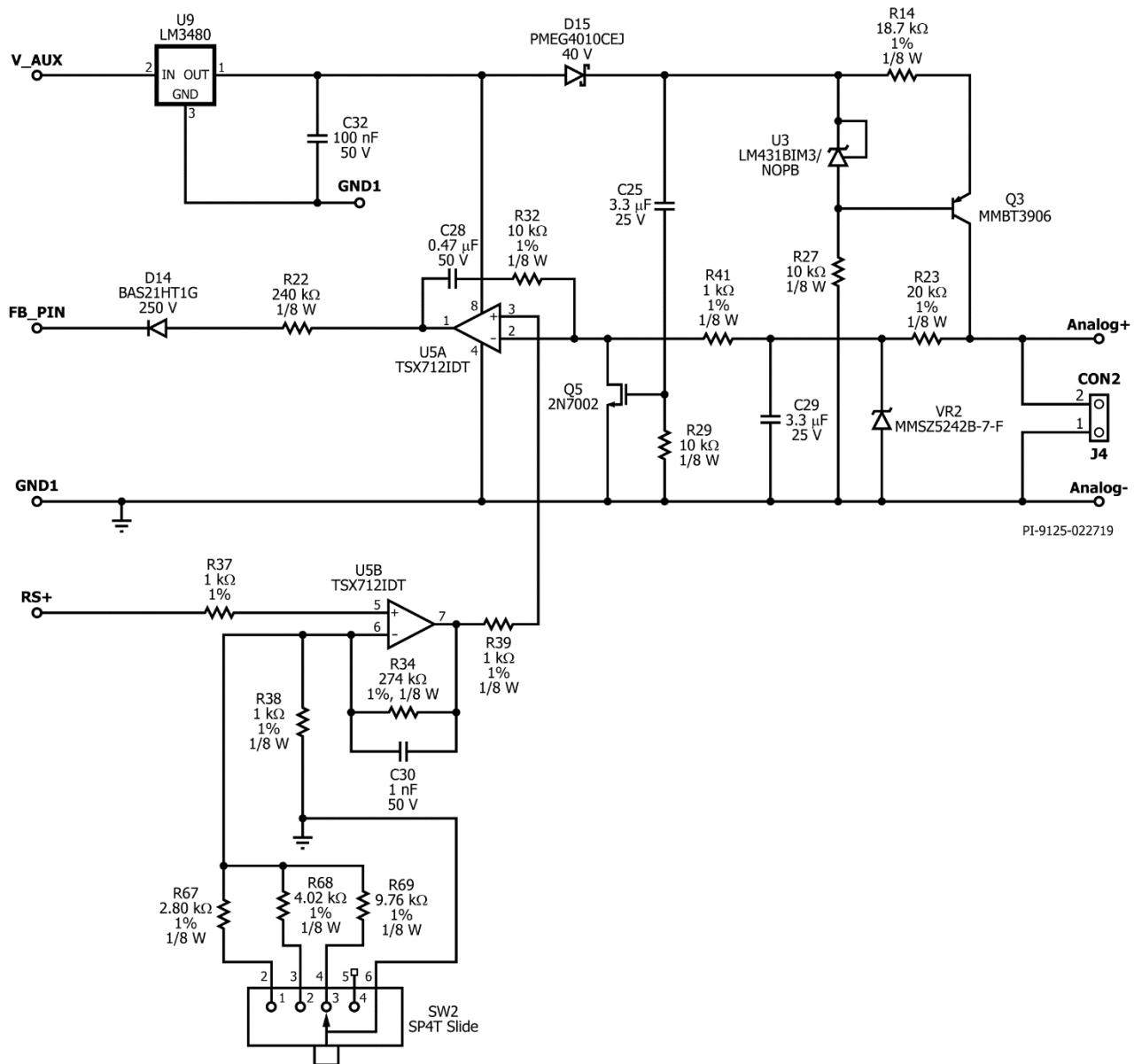


Figure 10 – 3-Way Dimming Control Schematic and Power Selection Schematic.

4.4.1 3-in-1 dimming control circuit function

The dimming control circuit basic function is sensing the output current, amplifying the signal and comparing it with a variable reference, and then injecting current into the FB pin to control the output regulation.

Output current is sensed through IS pin resistors R31 and R24. The output current passes through these resistors and the resulting voltage signal is then passed through the non-inverting amplifier circuit R37, R38, R34, U5B, and C30. The gain is set by R37 and R38 to 274 or about 9.5 V maximum. The output of the op-amp (pin 7) connects to the positive input (pin 3) through R39. The signal going to the negative input (pin 2) comes from variable resistance ($0\ \Omega - 100\ \text{k}\Omega$), or variable duty PWM signal (0% – 100%, 300 – 3 kHz) as dimming inputs.

The basic principle of the circuitry is that the output at pin 7 of U5B will always try to match the voltage at pin 2 of U5A which is set by the dimming input (0 V – 10 V DC). Since U5B is configured as a non-inverting op-amp and its input voltage signal is directly proportional to the output current, an increase in the voltage at pin 2 of U5A will result to an increase in the output current.

When the dimming input is a variable duty PWM signal, the averaging circuit composed of R23 and C29 converts the signal into DC before feeding to the op-amp input. A constant current source composed of R27, R14, U3, and Q3 is used to convert the variable resistance dimming input into the desired variable DC signal. Zener shunt regulator U3 clamps the voltage at R14, therefore setting the emitter current constant. The emitter current of Q3 is roughly equal to its collector current (around 100 μA) which is connected to the variable resistance input which in turn produces the 0 V – 10 V needed at pin 2 of U5A. VR2 is placed for protection in case the user has interchanged the dimming input causing inverted polarity.

At start-up, the op-amp output is initially low which causes an unwanted spike in output current. To prevent this sudden intensity in LED load, a blanking circuit, Q5, R29, and C25, is added which initially pulls the inverting input (pin 2) down and in turn results to op-amp output high. The op-amp output (pin 1) is connected to the FB pin through D14 and R22. Depending on the op-amp output, current is injected into the FB pin. The feedback voltage will go up as current is injected. This will normally bring the output voltage down in CV mode. However, since the LED load is a constant voltage, it cannot bring the voltage down. Instead, the output current goes down as a consequence. The current injection loop has to be slow enough in order not to trigger feedback overvoltage protection when doing a step load from 100% to 0%. This is done by increasing the value of R22.

The operational amplifier U5 is powered by the secondary winding FL3 and FL4 through LDO regulator, U9 with a 12 V DC rail output.



A low-input offset operational amplifier is also recommended to reduce unit-to-unit variability. It is also important to place the dimming circuit close to the IS pin and FB pin to prevent noise from disturbing the loop. An operational amplifier with better slew-rate like LT1638 can also help stabilize the dimming response especially at deep dimming. To use LT1638, loop compensation network is adjusted for better dimming response (see below schematic changes: C30 is removed and R32 is shorted). In terms of cost, LT1638 is more expensive than TSX712IDT.

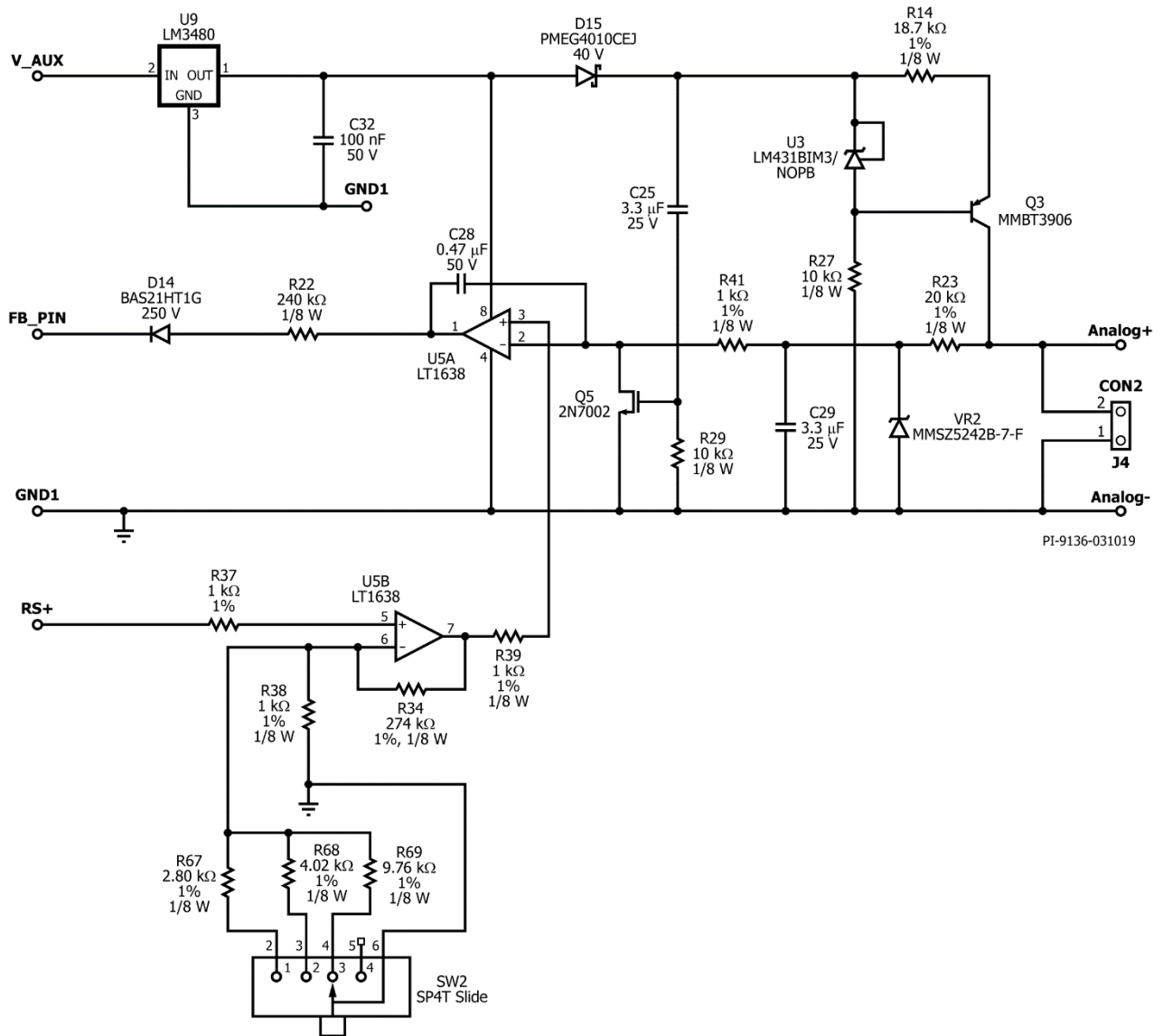
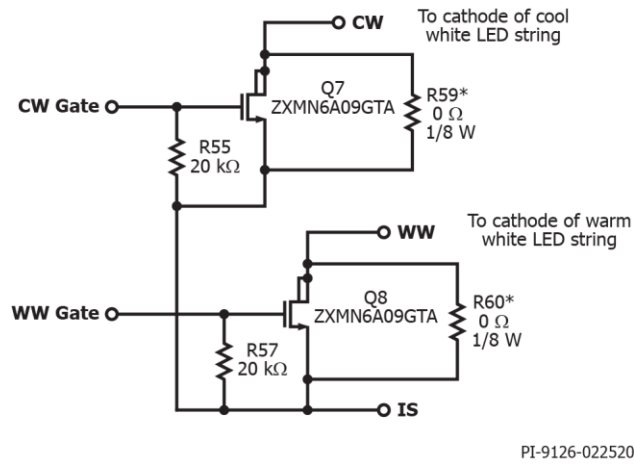


Figure 11 – Dimming Schematic Using LT1638.





CCT Selection

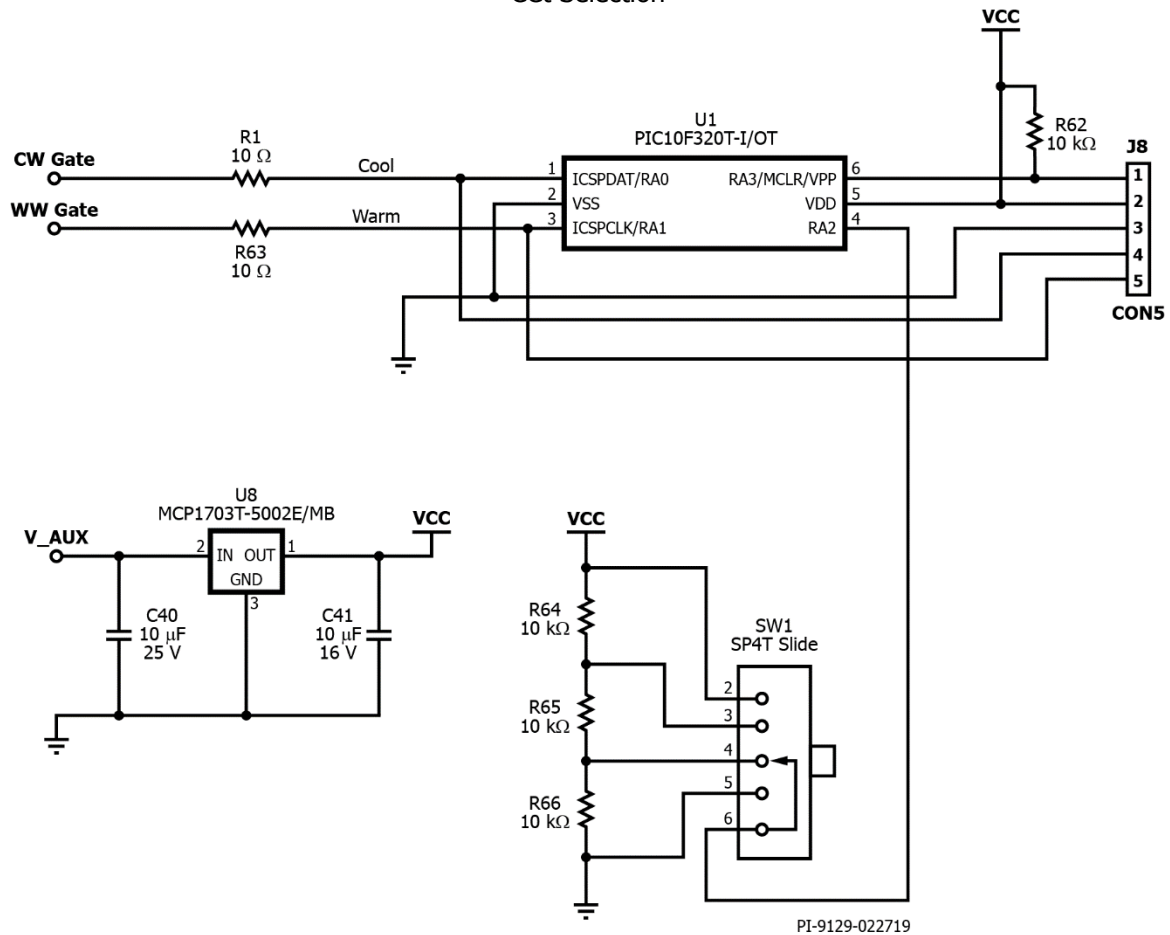


Figure 12 – Multi-Set and CCT Selection Schematic.

4.4.2 Power and CCT Selection

The daughter board is capable of power and CCT selection. For the software, use "PIC10F320_breakout_200Hz.hex" to program the microcontroller U1 via J8 header.

4.4.2.1 Power Selection

The LED ballast design has four power selections: 50 W, 45 W, 40 W, and 35 W. The power selection feature is done by varying the gain at the non-inverting amplifier U5B using a slide switch, SW2. Switch SW2 selects a parallel resistor across R38 from R67, 68, and 69, to set the desired gain and the output voltage of U5B. The change in gain also changes the error between pin 2 and pin 3 which changes the current injection in FB pin.

Since U5B is configured as a non-inverting op-amp and its input voltage signal is directly proportional to the output current, an increase in the voltage at pin 2 of U5A will result to an increase in the output current.

4.4.2.2 CCT Selection

The DER-847 board also features Correlated Color Temperature (CCT) function. CCT describes the color appearance of a white LED. CCT function allows the user to select among four color temperatures: 3000K (warm white), 3500K, 4000K, 5000K (neutral white).

The LED panel consists of one 5000K 36 V LED string while the second is 3000K 36V LED string. The LED color is changed using slide switch SW1, which selects the voltage fed to microcontroller, PIC10F320T, U1 through R64, R65, and R66. The voltage fed assigns the corresponding output PWM at U1 which drives each string via MOSFETs, Q7 and Q8, when selecting the desired combination of LED load string or output LED color temperature.

| CCT Selection | Duty Cycle (%) | |
|---------------|----------------|-----------|
| | PWM at Q7 | PWM at Q8 |
| 3000K | 0% | 100% |
| 3500K | 25% | 75% |
| 4000K | 50% | 50% |
| 5000K | 100% | 0% |

5 PCB Layout

5.1 Main Board Layout

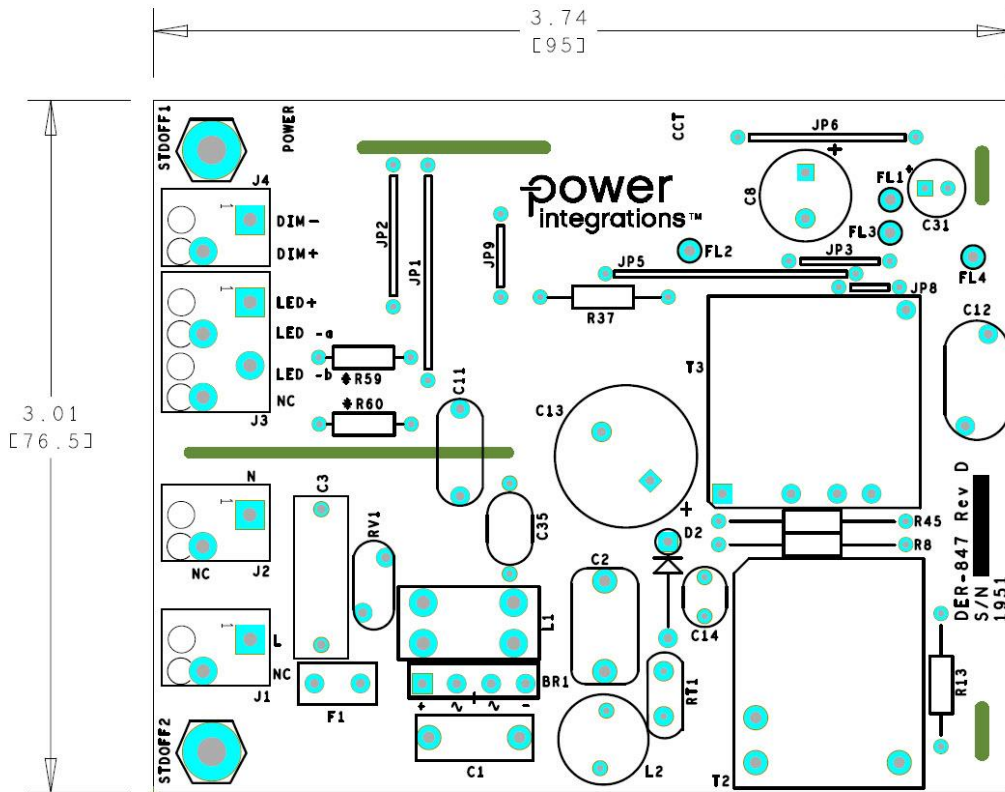


Figure 13 – PCB Top Side.

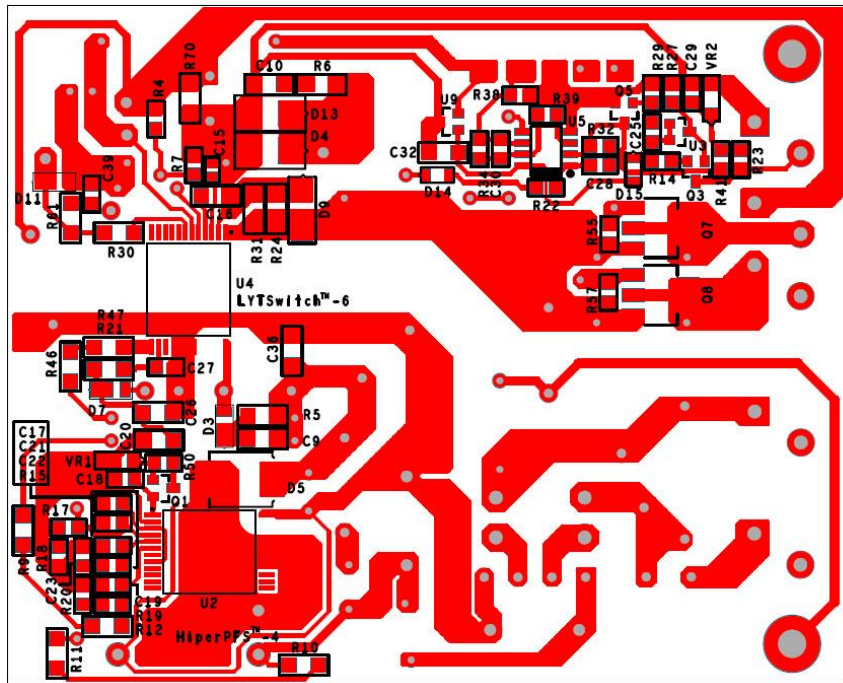


Figure 14 – PCB Bottom Side.



5.2 **Dimming Circuit Board Layout**

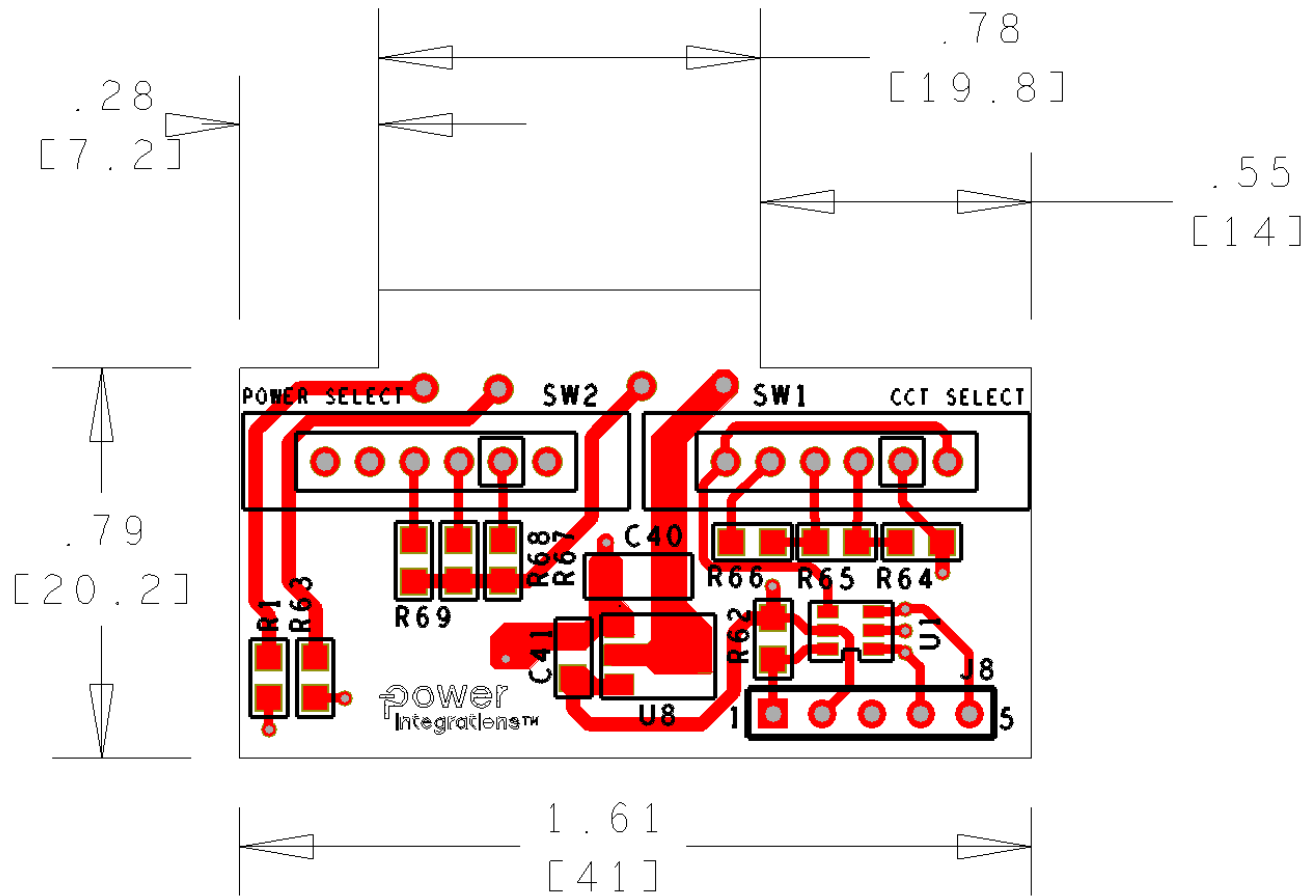


Figure 15 – PCB Top Side.

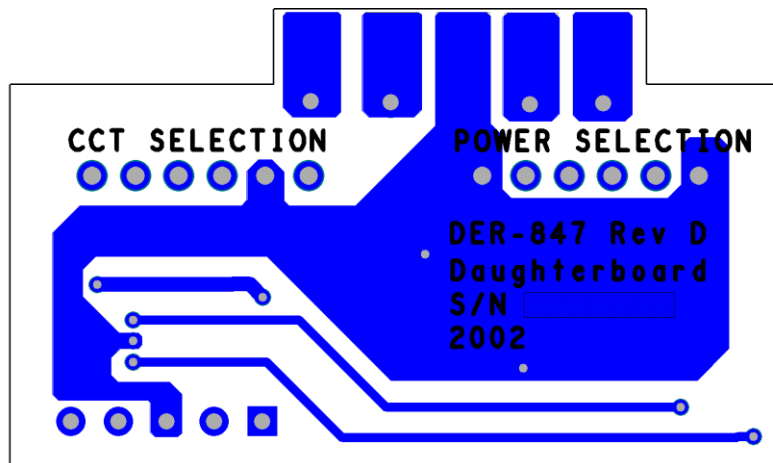


Figure 16 – PCB Bottom Side.

6 Bill of Materials

| Item | Qty | Ref Des | Description | Mfg Part Number | Mfg |
|------|-----|-----------------|---|----------------------|------------------|
| 1 | 1 | BR1 | Bridge Rectifier, 1000 V, 4 A, 4-ESIP, D3K, -55°C ~ 150°C (TJ), Vf=1V @ 7.5A | UD4KB100-BP | Micro Commercial |
| 2 | 1 | C1 | 100 nF, 450 V, Polypropylene Film | ECW-F2W104JAQ | Panasonic |
| 3 | 1 | C2 | 330 nF, 450 V, METALPOLYPRO | ECW-F2W334JAQ | Panasonic |
| 4 | 1 | C3 | 220 nF, ±10%, 275 VAC, Polypropylene Film, X2, 0.709" L x 0.236" W (18.00 mm x 6.00 mm) | 890324025027 | Würth |
| 5 | 1 | C8 | 330 µF, ALUM, 20%, 50 V, RADIAL, 10000 Hrs @ 105°C, 0.394" Dia (10.00 mm), 0.866" Height (22.00 mm), 0.197" LS (5.00 mm) | UHW1H331MPD | Nichicon |
| 6 | 1 | C9 | 1000 pF, 630 V, Ceramic, X7R, 1206 | C1206C102KBRCTU | Kemet |
| 7 | 1 | C10 | 220 pF, 630 V, Ceramic, NPO, 1206 | C3216C0G2J221J | TDK |
| 8 | 1 | C11 | 330 pF, Ceramic Y1 | 440LT33-R | Vishay |
| 9 | 1 | C12 | 3.3 nF, Ceramic, Y1 | 440LD33-R | Vishay |
| 10 | 1 | C13 | C22 µF, ±20%, 450 V, Aluminum, Radial, Can, 10000 Hrs @ 105°C, 0.630" Dia (16.00 mm), 0.787" H (20.00 mm), 0.295" LS (7.50 mm), 10000 Hrs @ 105°C | EEU-ED2W220S | Panasonic |
| 11 | 1 | C14 | 10 nF, 1 kV, Disc Ceramic, X7R | SV01AC103KAR | AVX |
| 12 | 1 | C15 | 330 pF 50 V, Ceramic, X7R, 0603 | CC0603KRX7R9BB331 | Yageo |
| 13 | 1 | C16 | 2.2 µF, 25 V, Ceramic, X7R, 1206 | TMK316B7225KL-T | Taiyo Yuden |
| 14 | 3 | C17 C18 C23 | 1 µF, ±10%, 50 V, Ceramic, X7R, Boardflex Sensitive, 0805, -55°C ~ 125°C | CGA4J3X7R1H105K125AE | TDK |
| 15 | 2 | C19 C21 | 470 pF, 50 V, Ceramic, X7R, 0805 | CC0805KRX7R9BB471 | Yageo |
| 16 | 2 | C20 C26 | 10 µF, 10%, 50 V, Ceramic, X7R, -55°C ~ 125°C, 1206, 0.126" L x 0.063" W (3.20 mm x 1.60 mm) | CL31B106KBHNNNE | Samsung |
| 17 | 1 | C22 | 100 nF, 25 V, Ceramic, X7R, 0805 | 08053C104KAT2A | AVX |
| 18 | 1 | C25, C29 | 3.3 µF, 25 V, Ceramic, X7R, 0805 | C2012X7R1E335K | TDK |
| 19 | 2 | C27 C28 | 0.47 µF, ±10%, 50 V, Ceramic, X7R, 0805, -55°C ~ 125°C | CGA4J3X7R1H474K125AB | TDK |
| 20 | 1 | C30 | 1 nF, 50 V, Ceramic, X7R, 0805 | 08055C102KAT2A | AVX |
| 21 | 1 | C31 | 47 µF, 50 V, Electrolytic, Gen. Purpose, (6.3 x 11) | EKMG500ELL470MF11D | United Chemi-Con |
| 22 | 1 | C32 | 100 nF, 50 V, Ceramic, X7R, 1206 | CC1206KRX7R9BB104 | Yageo |
| 23 | 1 | C35 | 47 pF ±10% Ceramic Disc, 760VAC (X1), 500 VAC (Y1), Y5S, -40°C ~ 125°C, X1, Y1, Safety | VY1470K31Y5SQ63V0 | Vishay |
| 24 | 1 | C36 | 10 nF, 630 V, Ceramic, X7R, 1206 | C1206C103KBRCTU | Kemet |
| 25 | 1 | C39 | 220 pF, ±10%, 200V, X7R, Ceramic, -55°C ~ 125°C, SMT, MLCC 0805 | CL21B221KDCNFNC | Samsung |
| 26 | 1 | C40 | 10 µF, 25 V, X7R, Ceramic, 1206 | C32116X7R1E106M160AB | TDK |
| 27 | 1 | C41 | 10 µF, ±10%, 16 V, X7R, Ceramic, SMT, MLCC 0805 | CL21B106KOQNNNE | Samsung |
| 28 | 1 | D2 | 800 V, 1 A, GP, Rectifier, DO-41 | 1N4006-E3/54 | Vishay |
| 29 | 1 | D3 | 600 V, 1 A, Rectifier, Glass Passivated, POWERDI123 | DFLR1600-7 | Diodes, Inc. |
| 30 | 2 | D4 D13 | 400 V, 2 A, Super-Fast, 35 ns, DO-214A, SMB | ES2G-13-F | Diodes, Inc. |
| 31 | 1 | D5 | 600 V, 3 A, SMC, DO-214AB | STTH3R06S | ST Micro |
| 32 | 1 | D7 | 400 V, 1 A, Rectifier, Glass Passivated, POWERDI123 | DFLR1400-7 | Diodes, Inc. |
| 33 | 1 | D9 | Diode, SCHOTTKY, 40 V, 3 A, SMA, DO-214AA | B340A-13-F | Diodes, Inc. |
| 34 | 1 | D11 | Diode, UFAST, 200 V, 1 A, POWERDI123 | DFLU1200-7 | Diodes, Inc. |
| 35 | 1 | D14 | Diode, General Purpose, Power, Switching, SS SWCH DIO, 250V, SC-76, SOD-323 | BAS21HT1G | ON Semi |
| 36 | 1 | D15 | Diode, SCHOTTKY, 40 V, 1A, SOD323F | PMEG4010CEJ,115 | NXP Semi |
| 37 | 1 | F1 | 3.15 A, 250V, Slow, RST | 507-1181 | Belfuse |
| 38 | 4 | FL1 FL2 FL3 FL4 | Flying Lead, Hole size 50mils | N/A | N/A |
| 39 | 3 | J1 J2 J4 | 2 Position (1 x 2), Wire to Board Terminal Block, | 1-2834011-2 | TE Connectivity |

| | | | | | |
|----|---|--------------------------------------|---|---------------------|--------------------------------|
| | | | Top Entry, Vertical with Board 0.138" (3.50 mm) Through Hole, Kinked Pins | | AMP Connectors |
| 40 | 1 | J3 | 4 Position (1 x 4), Wire to Board Terminal Block, Top Entry, Vertical with Board 0.138" (3.50 mm) Through Hole, Kinked Pins | 1-2834011-4 | TE Connectivity AMP Connectors |
| 41 | 1 | J8 | 5 Position (1 x 5) header, Unshrouded, 0.100" (2.54 mm) Through Hole, Tin, Vertical | MDF7-5P-2.54DSA(01) | Hirose Electric |
| 42 | 7 | JP1 JP2 JP3 JP5 JP6 JP8 JP9 | Wire Jumper, Non insulated, #28 AWG, 0.5 in | 299/2 SV001 | Alpha Wire |
| 43 | 1 | L1 | 10 mH, 0.7 A, Common Mode Choke | 744821110 | Würth |
| 44 | 1 | L2 | 680 μ H, Unshielded, Wirewound, Inductor, 650mA, 1.1 Ω Max, Radial | RCH110NP-681K | Sumida |
| 45 | 1 | Q1 | NPN, Small Signal BJT, 80 V, 0.5 A, SOT-23 | MMBTA06LT1G | On Semi |
| 46 | 1 | Q3 | PNP, Small Signal BJT, 40 V, 0.2 A, SOT-23 | MMBT3906LT1G | On Semi |
| 47 | 1 | Q5 | 60 V, 115 mA, SOT23-3 | 2N7002-7-F | Diodes, Inc. |
| 48 | 2 | Q7 Q8 | MOSFET, N-CH, 60V, 5.4A (Ta), TO-261-4, TO-261AA, SOT223 | ZXMN6A09GTA | Diodes, Inc. |
| 49 | 2 | R1 R63 | RES, 10 Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ100V | Panasonic |
| 50 | 1 | R4 | RES, 499 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF4993V | Panasonic |
| 51 | 2 | R5 R46 | RES, 1.00 M Ω , 1%, 1/4 W, Thick Film, 1206 | ERJ-8ENF1004V | Panasonic |
| 52 | 2 | R6 R61 | RES, 20 Ω , 1%, 1/4 W, Thick Film, 1206 | ERJ-8ENF20R0V | Panasonic |
| 53 | 1 | R7 | RES, 15.4 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1542V | Panasonic |
| 54 | 2 | R8 R13 | RES, 3.74 M Ω , 1%, 1/4 W, Metal Film | MFR-25FBF52-3M74 | Yageo |
| 55 | 4 | R9 R10 R11 R12 | RES, 6.2 M Ω , 1%, 1/4 W, Thick Film, 1206 | KTR18EZPF6204 | Rohm Semi |
| 56 | 1 | R14 | RES, 18.7 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1872V | Panasonic |
| 57 | 1 | R15 | RES, 30.1 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF3012V | Panasonic |
| 58 | 2 | R17 R19 | RES, 9.09 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF9091V | Panasonic |
| 59 | 2 | R18 R20 | RES, 143 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1433V | Panasonic |
| 60 | 1 | R21 | RES, 10 k Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ103V | Panasonic |
| 61 | 1 | R22 | RES, 240 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ244V | Panasonic |
| 62 | 1 | R23 | RES, 20.0 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF2002V | Panasonic |
| 63 | 1 | R24 | RES, SMD, 0.068, 68 m Ω , \pm 1%, 1/2W, 1206, Current Sense, Moisture Resistant Thick Film | RL1206FR-7W0R068L | Yageo |
| 64 | 6 | R27 R29 R62 R64 R65 R66 | RES, 10 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ103V | Panasonic |
| 65 | 1 | R30 | RES, 47 Ω , 5%, 1/4 W, Thick Film, 1206 | ERJ-8GEYJ470V | Panasonic |
| 66 | 1 | R31 | RES, SMD, 0.05 Ω , 1%, 1/2 W, 1206, \pm 100ppm/ $^{\circ}$ C, -55 $^{\circ}$ C ~ 155 $^{\circ}$ C | CSR1206FT50L0 | Stackpole |
| 67 | 1 | R32 | RES, 10.0 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1002V | Panasonic |
| 68 | 1 | R34 | RES, 274 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF2743V | Panasonic |
| 69 | 1 | R37 | RES, 1 k Ω , 1%, 1/4 W, Metal Film | MFR-25FBF-1K00 | Yageo |
| 70 | 3 | R38 R39 R41 | RES, 1.00 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF1001V | Panasonic |
| 71 | 1 | R45 | RES, 1 M Ω , 1%, 1/4 W, Metal Film | MFR-25FBF-1M00 | Yageo |
| 72 | 1 | R47 | RES, 1.91 M Ω , 1%, 1/4 W, Thick Film, 1206 | RMCF1206FT1M91 | Stackpole |
| 73 | 1 | R50 | RES, 30 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ303V | Panasonic |
| 74 | 2 | R55 R57 | RES, 20 k Ω , 5%, 1/8 W, Thick Film, 0805 | ERJ-6GEYJ203V | Panasonic |
| 75 | 2 | R59 R60 | RES, 0 Ω , 5%, 1/4 W, Carbon Film | ZOR-25-B-52-0R | Yageo |
| 76 | 1 | R67 | RES, 2.80 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF2801V | Panasonic |
| 77 | 1 | R68 | RES, 4.02 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF4021V | Panasonic |
| 78 | 1 | R69 | RES, 9.76 k Ω , 1%, 1/8 W, Thick Film, 0805 | ERJ-6ENF9761V | Panasonic |
| 79 | 1 | R70 | RES, 100 k Ω , 1%, 1/4 W, Thick Film, 1206 | ERJ-8ENF1003V | Panasonic |
| 80 | 1 | RT1 | NTC Thermistor, 2.5 Ω , 3 A | SL08 2R503 | Ametherm |
| 81 | 1 | RV1 | 300 VAC, 25 J, 7 mm, RADIAL | V300LA4P | Littlefuse |



| | | | | | |
|----|---|--------------------|--|--------------------|----------------------|
| 82 | 2 | STDOFF1 STDOFF2 | Standoff Hex,6-32, .375L, F/F, NYL, 94V-0 | 8441B | Keystone |
| 83 | 2 | SW1 SW2 | Slide Switch, SP4T,300MA, 125V TH, Vertical | SLB1470 | APE. |
| 84 | 1 | T2 | Bobbin, EE25, Vertical, 10 pins | YW-360-02B | Yih-Hwa |
| 85 | 1 | T3 | Bobbin, PQ20/20, Vertical, 14 pins | CPV-PQ20/20-1S14PZ | Ferroxcube |
| 86 | 1 | U1 | IC, PIC, PIC®, 10F Microcontroller, IC, 8-Bit, 16MHz, 448B (256 x 14) FLASH ,SOT236,SOT-23-6 | PIC10F320T-I/OT | Microchip Technology |
| 87 | 1 | U2 | HiperPFS-4,inSOP-24B | PFS7623C | Power Integrations |
| 88 | 1 | U3 | IC, REG ZENER SHUNT ADJ SOT-23 | LM431BIM3/NOPB | National Semi |
| 89 | 1 | U4 | LYTSwitch-6 Integrated Circuit, InSOP24D | LYT6067C | Power Integrations |
| 90 | 1 | U5 | IC, DUAL Op Amp, General Purpose, 2.7 MHz, Rail to Rail,8-SOIC (0.154", 3.90mm Width),8-SO | TSX712IDT | ST Micro |
| 91 | 1 | U8 | IC, Linear Voltage Regulator, Positive, Fixed, 1 Output, 5 V, 0.25 A, SOT-89-3,TO-243AA | MCP1703T-5002E/MB | Microchip Technology |
| 92 | 1 | U9 | IC, REG, LDO, 12V, 0.1A, SOT23-3 | LM3480IM3-12/NOPB | Texas Instruments |
| 93 | 1 | VR1 | 13 V, 5%, 500 mW, SOD-123 | MMSZ4700T1G | ON Semi |
| 94 | 1 | VR2 | DIODE ZENER 12 V 500 mW SOD123 | MMSZ5242B-7-F | Diodes, Inc. |

7 PFC Inductor (T2) Specifications

7.1 Electrical Diagram

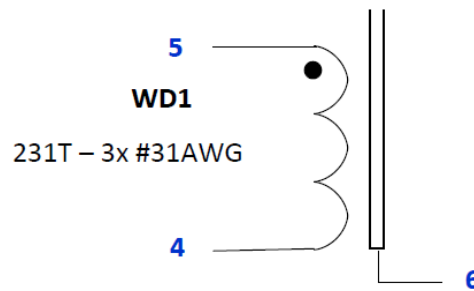


Figure 17 – Inductor Electrical Diagram.

7.2 Electrical Specifications

| Parameter | Condition | Spec. |
|----------------------------|--|--------------|
| Nominal Primary Inductance | Measured at 1 V _{PK-PK} , 100 kHz switching frequency, between pin 4 and pin 5, with all other windings open. | 1806 μ H |
| Tolerance | Tolerance of Primary Inductance. | \pm 5% |

7.3 Material List

| Item | Description |
|------|---------------------------------|
| [1] | Core: EE25. |
| [2] | Bobbin, EE25, Vertical, 10 pin. |
| [3] | Magnet Wire: #31 AWG. |
| [4] | Polyester Tape: 8.7 mm. |
| [5] | Polyester Tape: 11 mm. |
| [6] | Copper Wire. |

7.4 Inductor Build Diagram

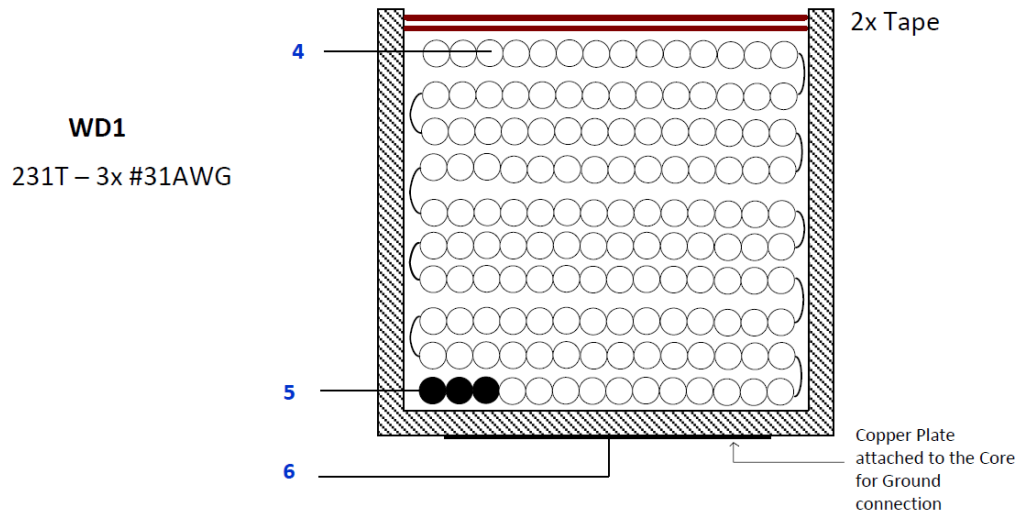






Figure 18 – Transformer Build Diagram.

7.5 Inductor Construction

| | |
|---------------------------|--|
| Winding Directions | Bobbin is oriented on winder jig such that terminal pin 1-5 is on the left side. The winding direction is clockwise. |
| Winding 1 | Use 3-layer magnetic wire Item [3]. Start at pin 5 and wind 231 turns then finish the winding on pin 4. |
| Insulation | Apply 2 layers of polyester tape, Item [5] for insulation. |
| Core Grinding | Grind the center leg of 1 core to meet the nominal inductance specification 1806 μ H. |
| Assemble Core | Assemble the 2 cores into the bobbin. |
| Core Termination | Prepare a copper strip with a soldered magnetic wire, Item [6], at the middle as shown in the picture. Apply copper strip at the bottom part of the core and terminate the magnetic wire on Pin 6. |
| Bobbin Tape | Add 2 layers of polyester tape Item [4] around the bobbin together with the core to fix the 2 cores. |
| Pins | Cut terminal pins 1, 2, 3, 7, 8, 9, and 10. |
| Finish | Apply 2:1 varnish and thinner solution. |

7.6 **Winding Illustrations**

| | |
|--|--|
| <p>Winding Directions</p> <p>Bobbin is oriented on winder jig such that terminal pin 1-5 is on the left side. The winding direction is clockwise.</p> |  |
| <p>Winding 1</p> <p>Use 3-layer magnetic wire Item [3]. Start at pin 5 and wind 231 turns then finish the winding on pin 4.</p> |  |
| <p>Insulation</p> <p>Apply 2 layers of polyester tape, Item [5] for insulation.</p> |  |
| <p>Core Grinding</p> <p>Grind the center leg of 1 core to meet the nominal inductance specification 1806 μH.</p> |  |

| | |
|--|---|
| <p>Assemble Core</p> <p>Assemble the 2 cores into the bobbin</p> |  |
| <p>Core Termination</p> <p>Prepare a copper strip with a soldered magnetic wire, Item [6], at the middle as shown in the picture. Apply copper strip at the bottom part of the core and terminate the magnetic wire on pin 6.</p> |  |
| <p>Bobbin Tape</p> <p>Add 2 layers of polyester tape Item [4] around the bobbin together with the core to fix the 2 cores.</p> |  |
| <p>Pins</p> <p>Cut terminal pins 1, 2, 3, 7, 8, 9, and 10.</p> <p>Finish</p> <p>Apply 2:1 varnish and thinner solution.</p> |  |

8 Flyback Transformer (T3) Specifications

8.1 Electrical Diagram

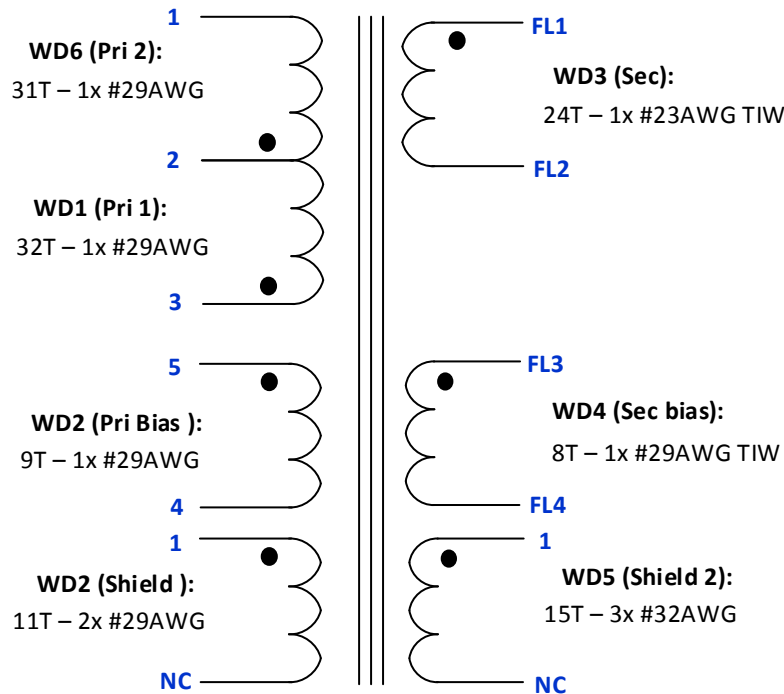


Figure 19 – Transformer Electrical Diagram.

8.2 Electrical Specifications

| Parameter | Condition | Spec. |
|----------------------------|---|--------|
| Nominal Primary Inductance | Measured at 1 V _{PK-PK} , 100 kHz switching frequency, across pin 1 and pin 3, with all other windings open. | 871 μH |
| Tolerance | Tolerance of Primary Inductance. | ±5% |
| Leakage Inductance | Short all bias windings and secondary windings. Measured at 1 V _{PK-PK} , 100 kHz switching frequency, across pin 1 and pin 3. | <5 μH |

8.3 Material List

| Item | Description |
|------|-----------------------------------|
| [1] | Core: PQ2020 Equivalent. |
| [2] | Bobbin: PQ2020, Vertical, 14 pin. |
| [3] | Primary Magnet Wire: #29 AWG. |
| [4] | Shield Magnet Wire: #32 AWG. |
| [5] | Secondary Wire TIW: # 23 AWG. |
| [6] | Auxiliary Wire TIW: # 29 AWG. |
| [7] | Polyester Tape: 11.5 mm. |
| [8] | Polyester Tape: 9.3 mm. |

8.4 **Transformer Build Diagram**

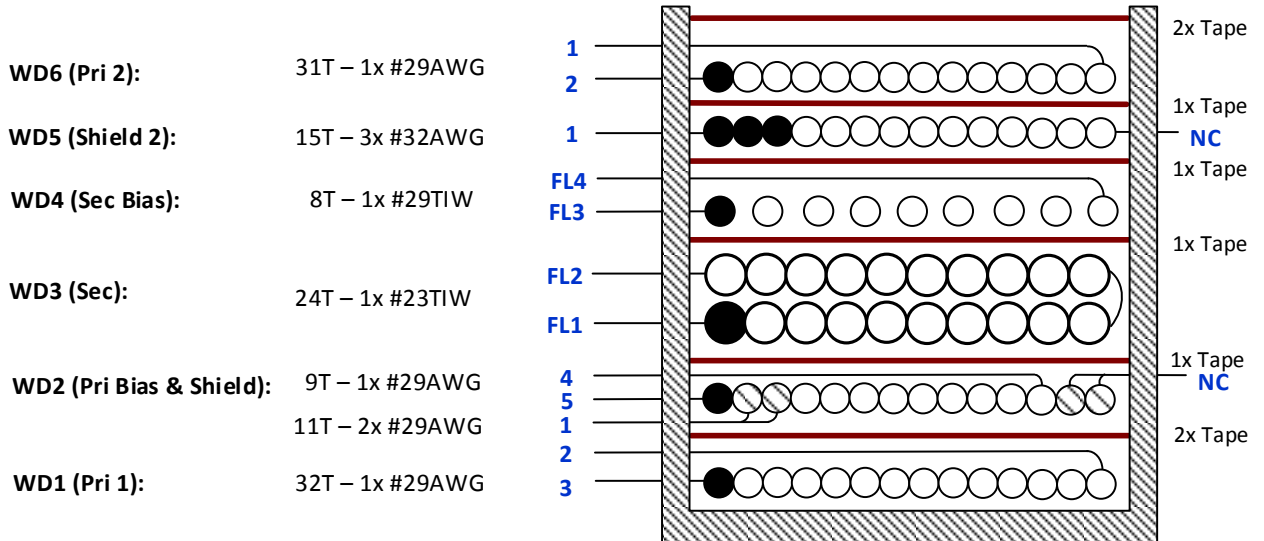



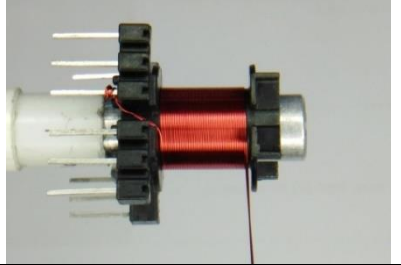
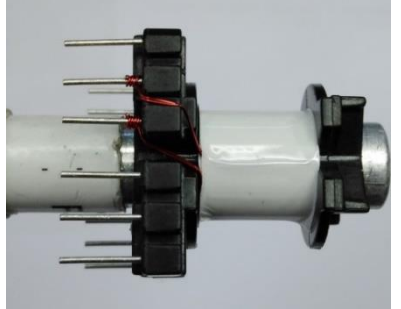
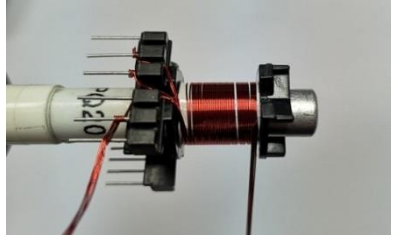
Figure 20 – Inductor Build Diagram.

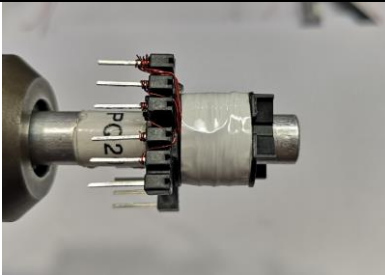
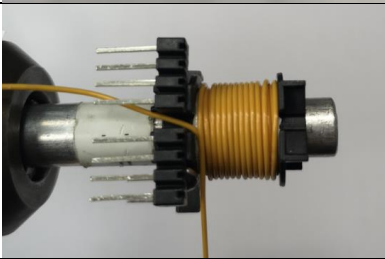
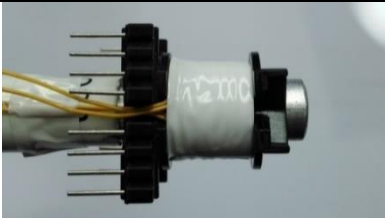
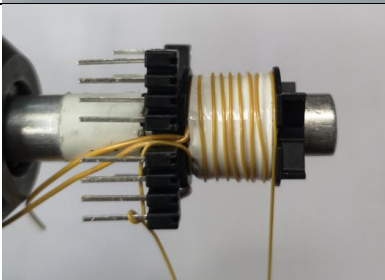
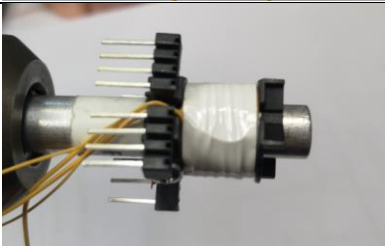
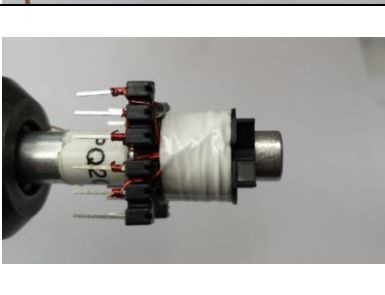
8.5 **Transformer Construction**

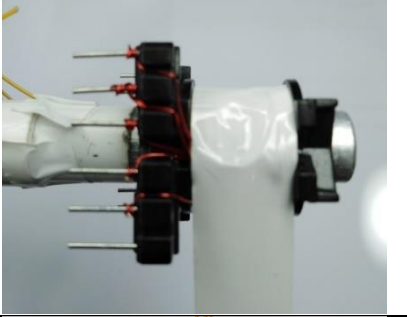

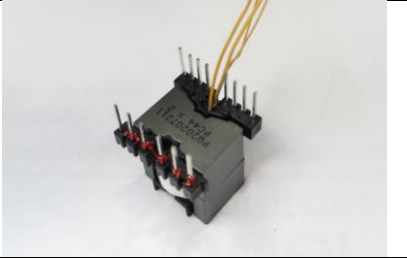
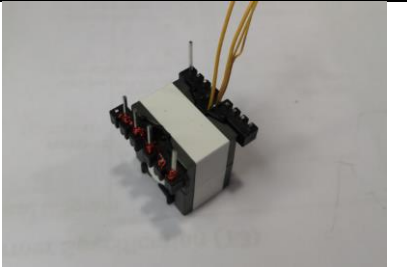
| | |
|---------------------------|---|
| Winding Directions | Bobbin is oriented on winder jig such that terminal pin 1-6 is on the left side. The winding direction is clockwise. |
| Winding 1 | Use magnetic wire Item [3]. Start at pin 3 and wind 32 turns evenly. Finish the winding on pin 2. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Winding 2 | Use 1-layer magnetic wire Item 3. Start at pin 5. Use 2-layer magnetic wire item 3 and start at pin 1. Wind both wires 9 turns and 11 turns respectively. Terminate the 1-layer winding (9T) to pin 4. Float the 2-layer winding (11T) on the other side of bobbin. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Winding 3 | Use 1-layer triple insulated wire Item [5] and mark the start terminal as FL1. Start at FL1 and wind 12 turns in 1 layer. Continue 12T on the next layer of secondary winding. Finish winding and mark as FL2. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Winding 4 | Use 1-layer triple-insulated wire Item [6]. Mark and start terminal at FL3 and wind 8 turns evenly. Finish and mark the winding at FL4. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Winding 5 | Use 3-layer magnetic wire Item [4]. Start at pin 1 and wind 15 turns evenly. Finish the winding as floating wire on the other side of bobbin. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Winding 6 | Use magnetic wire Item [3]. Start at pin 2 and wind 31 turns evenly. Finish the winding on pin 1. |
| Insulation | Apply 1 layer of polyester tape, Item [7] for insulation. |
| Core Grinding | Grind the center leg of 1 core to meet the nominal inductance specification of 871 μ H. |
| Assemble Core | Assemble the 2 cores into the bobbin and secure with polyester tape Item [8]. |
| Pins | Cut terminal pins 6, 8 to 14 and half of pin 2. |
| Apply Varnish | Apply 2:1 varnish and thinner solution. |



8.6 **Winding Illustrations**

| | |
|--|--|
| <p>Winding Directions</p> <p>Bobbin is oriented on winder jig such that terminal pin 1-6 is on the left side. The winding direction is clockwise.</p> |  |
| <p>Winding 1</p> <p>Use magnetic wire Item [3]. Start at pin 3 and wind 32 turns evenly. Finish the winding on pin 2.</p> |  |
| <p>Insulation</p> <p>Apply 1 layer of polyester tape, Item [7] for insulation.</p> |  |
| <p>Winding 2</p> <p>Use 1-layer magnetic wire Item 3. Start at pin 5. Use 2-layer magnetic wire item 3 and start at pin 1. Wind both wires 9 turns and 11 turns respectively. Terminate the 1-layer winding (9T) to pin 4. Float the 2-layer winding (11T) on the other side of bobbin.</p> |  |

| | |
|--|---|
| <p>Insulation</p> <p>Apply 1 layer of polyester tape, Item [7] for insulation.</p> |  |
| <p>Winding 3</p> <p>Use 1-layer triple insulated wire Item [5] and mark the start terminal as FL1. Start at FL1 and wind 12 turns in 1 layer. Continue 12T on the next layer of secondary winding. Finish winding and mark as FL2.</p> |  |
| <p>Insulation</p> <p>Apply 1 layer of polyester tape, Item [7] for insulation.</p> |  |
| <p>Winding 4</p> <p>Use 1-layer triple-insulated wire Item [6]. Mark and start terminal at FL3 and wind 8 turns evenly. Finish and mark the winding at FL4.</p> |  |
| <p>Insulation</p> <p>Apply 1 layer of polyester tape, Item [7] for insulation.</p> |  |
| <p>Winding 5</p> <p>Use 3-layer magnetic wire Item [4]. Start at pin 1 and wind 15 turns evenly. Finish the winding as floating wire on the other side of bobbin.</p> <p>Insulation</p> <p>Apply 1 layer of polyester tape, Item [7] for insulation.</p> |  |

| | |
|---|---|
| <p>Winding 6</p> <p>Use magnetic wire Item [3]. Start at pin 2 and wind 31 turns evenly. Finish the winding on pin 1.</p> <p>Insulation</p> <p>Apply 2 layers of polyester tape, Item [7] for insulation.</p> |  |
| <p>Core Grinding</p> <p>Grind the center leg of 1 core to meet the nominal inductance specification of 871 μH.</p> |  |
| <p>Assemble Core</p> <p>Assemble the 2 cores into the bobbin and secure with polyester tape Item [8].</p> |  |
| <p>Pins</p> <p>Cut terminal pins 6, 8 to 14 and half of pin 2.</p> <p>Apply Varnish</p> <p>Apply 2:1 varnish and thinner solution.</p> |  |

9 PFC Boost Inductor Design Spreadsheet

| 1 | Hiper_PFS-4_Boost_051319; Rev.1.2; Copyright Power Integrations 2019 | INPUT | INFO | OUTPUT | UNITS | Continuous Mode Boost Converter Design Spreadsheet |
|----|--|-----------|------|-----------|-------|--|
| 2 | Enter Application Variables | | | | | |
| 3 | Input Voltage Range | Universal | | Universal | | Input voltage range |
| 4 | VACMIN | 100 | | 100 | VAC | Minimum AC input voltage. Spreadsheet simulation is performed at this voltage. To examine operation at other voltages, enter here, but enter fixed value for LPFC_ACTUAL. |
| 5 | VACMAX | 277 | | 277 | VAC | Maximum AC input voltage |
| 6 | VBROWNIN | | Info | 84 | VAC | Brown-IN voltage has been modified since the V-pin ratio is no longer 100:1 |
| 7 | VBROWNOUT | | Info | 73 | VAC | Brown-OUT voltage has been modified since the V-pin ratio is no longer 100:1 |
| 8 | VO | 410 | Info | 410 | VDC | Brown IN/OUT voltage has changed due to modifications in the V-pin ratio from 100:1. Recommend Vpin ratio= FB pin ratio for optimized operation. Check the PF, input current distortion, brown in/out and power delivery |
| 9 | PO | 54 | | 54 | W | Nominal Output power |
| 10 | fL | | | 50 | Hz | Line frequency |
| 11 | TA Max | | | 40 | °C | Maximum ambient temperature |
| 12 | Efficiency Estimate | 0.97 | | 0.97 | | Enter the efficiency estimate for the boost converter at VACMIN. Should approximately match calculated efficiency in Loss Budget section |
| 13 | VO_MIN | | | 390 | VDC | Minimum Output voltage |
| 14 | VO_RIPPLE_MAX | | | 20 | VDC | Maximum Output voltage ripple |
| 15 | T_HOLDUP | | | 20 | ms | Holdup time |
| 16 | VHOLDUP_MIN | | | 328 | VDC | Minimum Voltage Output can drop to during holdup |
| 17 | I_INRUSH | | | 40 | A | Maximum allowable inrush current |
| 18 | Forced Air Cooling | No | | No | | Enter "Yes" for Forced air cooling. Otherwise enter "No". Forced air reduces acceptable choke current density and core autpick core size |
| 20 | KP and INDUCTANCE | | | | | |
| 21 | KP_TARGET | 0.75 | | 0.75 | | Target ripple to peak inductor current ratio at the peak of VACMIN. Affects inductance value |
| 22 | LPFC_TARGET (0 bias) | | | 1806 | uH | PFC inductance required to hit KP_TARGET at peak of VACMIN and full load |
| 23 | LPFC_DESIRE (0 bias) | | Info | 1806 | uH | Inductance too high: Core size will be too big |
| 24 | KP_ACTUAL | | | 0.753 | | Actual KP calculated from LPFC_DESIRE |
| 25 | LPFC_PEAK | | | 1806 | uH | Inductance at VACMIN and maximum bias current. For Ferrite, same as LPFC_DESIRE (0 bias) |
| 27 | Basic current parameters | | | | | |
| 28 | IAC_RMS | | | 0.56 | A | AC input RMS current at VACMIN and Full Power load |
| 29 | IO_DC | | | 0.13 | A | Output average current/Average diode current |
| 32 | PFS Parameters | | | | | |
| 33 | PFS Package | C | | C | | HiperPFS package selection |
| 34 | PFS Part Number | PFS7623C | | PFS7623C | | If examining brownout operation, |

| | | | | | | |
|-----------|------------------------------------|------------|---------|------------|--------|---|
| | | | | | | over-ride autopick with desired device size |
| 35 | Operating Mode | Full Power | | Full Power | | Mode of operation of PFS. For Full Power mode enter "Full Power" otherwise enter "EFFICIENCY" to indicate efficiency mode |
| 36 | IOCP min | | | 3.80 | A | Minimum Current limit |
| 37 | IOCP typ | | | 4.10 | A | Typical current limit |
| 38 | IOCP max | | | 4.30 | A | Maximum current limit |
| 39 | IP | | | 1.25 | A | MOSFET peak current |
| 40 | IRMS | | | 0.52 | A | PFS MOSFET RMS current |
| 41 | RDSOn | | | 0.87 | Ohms | Typical RDSon at 100 °C |
| 42 | FS_PK | | | 54.0 | kHz | Estimated frequency of operation at crest of input voltage (at VACMIN) |
| 43 | FS_AVG | | | 44.5 | kHz | Estimated average frequency of operation over line cycle (at VACMIN) |
| 44 | PCOND_LOSS_PFS | | | 0.234 | W | Estimated PFS conduction losses |
| 45 | PSW_LOSS_PFS | | | 1.230 | W | Estimated PFS switching losses |
| 46 | PFS_TOTAL | | | 1.464 | W | Total Estimated PFS losses |
| 47 | TJ Max | | | 100 | deg C | Maximum steady-state junction temperature |
| 48 | Rth-JS | | | 2.80 | °C/W | Maximum thermal resistance (Junction to heatsink) |
| 49 | HEATSINK Theta-CA | | | 38.18 | °C/W | Maximum thermal resistance of heatsink |
| 52 | INDUCTOR DESIGN | | | | | |
| 53 | Basic Inductor Parameters | | | | | |
| 54 | LPFC (0 Bias) | | | 1806 | uH | Value of PFC inductor at zero current. This is the value measured with LCR meter. For powder, it will be different than LPFC. |
| 55 | LP_TOL | | | 10.0 | % | Tolerance of PFC Inductor Value (ferrite only) |
| 56 | IL_RMS | | | 0.61 | A | Inductor RMS current (calculated at VACMIN and Full Power Load) |
| 57 | Material and Dimensions | | | | | |
| 58 | Core Type | Ferrite | | Ferrite | | Enter "Sendust", "Iron Powder" or "Ferrite" |
| 59 | Core Material | PC44/PC95 | | PC44/PC95 | | Select from 60u, 75u, 90u or 125 u for Sendust cores. Fixed at PC44/PC95 for Ferrite cores. Fixed at -52 material for Pow Iron cores. |
| 60 | Core Geometry | EE | | EE | | Toroid only for Sendust and Powdered Iron; EE or PQ for Ferrite cores. |
| 61 | Core | EE25.4 | | EE25.4 | | Core part number |
| 62 | Ae | 51.40 | | 51.40 | mm^2 | Core cross sectional area |
| 63 | Le | 57.80 | | 57.80 | mm | Core mean path length |
| 64 | AL | 1250.00 | | 1250.00 | nH/t^2 | Core AL value |
| 65 | Ve | 2.97 | | 2.97 | cm^3 | Core volume |
| 66 | HT (EE/PQ/EQ/RM/POT) / ID (toroid) | 16.10 | | 16.10 | mm | Core height/Height of window; ID if toroid |
| 67 | MLT | 36.8 | | 36.8 | mm | Mean length per turn |
| 68 | BW | 4.01 | | 4.01 | mm | Bobbin width |
| 69 | LG | 1.57 | | 1.57 | mm | Gap length (Ferrite cores only) |
| 70 | Flux and MMF calculations | | | | | |
| 71 | BP_TARGET (ferrite only) | 7200 | Info | 7200 | Gauss | Info: Peak flux density is too high. Check for Inductor saturation during line transient operation |
| 72 | B_OCP (or BP) | | Warning | 7194 | Gauss | Warning: Peak flux density is too high. Check for Inductor saturation during load steps |
| 73 | B_MAX | | | 1908 | Gauss | Peak flux density at AC peak, VACMIN and Full Power Load, nominal |



| | | | | | | |
|------------|-----------------------------|----------|------|-----------|-------------------|---|
| | | | | | | inductance,minimum IOCP |
| 74 | μ _TARGET (powder only) | | | N/A | % | target μ at peak current divided by μ at zero current, at VACMIN, full load (powder only) - drives auto core selection |
| 75 | μ _MAX (powder only) | | | N/A | % | actual μ at peak current divided by μ at zero current, at VACMIN, full load (powder only) |
| 76 | μ _OCP (powder only) | | | N/A | % | μ at IOCPtyp divided by μ at zero current |
| 77 | I_TEST | 2.1 | | 2.1 | A | Current at which B_TEST and H_TEST are calculated, for checking flux at a current other than IOCP or IP; if blank IOCP_typ is used. |
| 78 | B_TEST | | | 3513 | Gauss | Flux density at I_TEST and maximum tolerance inductance |
| 79 | μ _TEST (powder only) | | | N/A | % | μ at IOCP divided by μ at zero current, at IOCPtyp |
| 80 | Wire | | | | | |
| 81 | TURNS | | | 231 | | Inductor turns. To adjust turns, change BP_TARGET (ferrite) or μ _TARGET (powder) |
| 82 | ILRMS | | | 0.61 | A | Inductor RMS current |
| 83 | Wire type | Magnet | | Magnet | | Select between "Litz" or "Magnet" for double coated magnet wire |
| 84 | AWG | 31 | Info | 31 | AWG | Selected wire has increased losses due to skin and proximity effects. Consider using multiple strands of thinner wires, Litz wire, or decreasing the number of layers |
| 85 | Filar | 3 | | 3 | | Inductor wire number of parallel strands. Leave blank to auto-calc for Litz |
| 86 | OD (per strand) | | | 0.226 | mm | Outer diameter of single strand of wire |
| 87 | OD bundle (Litz only) | | | N/A | mm | Will be different than OD if Litz |
| 88 | DCR | | | 1.574 | ohm | Choke DC Resistance |
| 89 | P AC Resistance Ratio | | Info | 16.14 | | AC resistance is high. Check copper loss, use Litz or thinner wire and fewer layers, or reduce Kp |
| 90 | J | | | 5.08 | A/mm ² | Estimated current density of wires. It is recommended that $4 < J < 6$ |
| 91 | FIT | | | 68 | % | Percentage fill of winding window for EE/PQ core. Full window approx. 90% |
| 92 | Layers | | | 48.64 | | Estimated layers in winding |
| 93 | Loss calculations | | | | | |
| 94 | BAC-p-p | | | 1437 | Gauss | Core AC peak-peak flux excursion at VACMIN, peak of sine wave |
| 95 | LPFC_CORE_LOSS | | | 0.024 | W | Estimated Inductor core Loss |
| 96 | LPFC_COPPER_LOSS | | Info | 9.491 | W | Info: Copper loss too high. Adjust wire gauge and/or filar, being mindful of AC Resistance ratio |
| 97 | LPFC_TOTAL_LOSS | | Info | 9.514 | W | Total losses too high |
| 100 | External PFC Diode | | | | | |
| 101 | PFC Diode Part Number | STTH3R06 | | STTH3R06 | | PFC Diode Part Number |
| 102 | Type / Part Number | | | ULTRAFast | | PFC Diode Type / Part Number |
| 103 | Manufacturer | | | ST | | Diode Manufacturer |
| 104 | VRRM | | | 600.0 | V | Diode rated reverse voltage |
| 105 | IF | | | 3.00 | A | Diode rated forward current |
| 106 | Qrr | | Info | 190.0 | nC | Qrr too high: Will result in high diode loss |
| 107 | VF | | | 1.25 | V | Diode rated forward voltage drop |
| 108 | PCOND_DIODE | | | 0.170 | W | Estimated Diode conduction losses |
| 109 | PSW_DIODE | | | 0.300 | W | Estimated Diode switching losses |

| | | | | | | |
|------------|---|----|---------|--------|-------------------|--|
| 110 | P_DIODE | | | 0.471 | W | Total estimated Diode losses |
| 111 | TJ Max | | | 100.0 | deg C | Maximum steady-state operating temperature |
| 112 | Rth-JS | | Info | 20.00 | degC/W | Rth too high. Will result in high diode loss |
| 113 | HEATSINK Theta-CA | | | 106.96 | degC/W | Maximum thermal resistance of heatsink |
| 114 | IFSM | | | 55.0 | A | Non-repetitive peak surge current rating. Consider larger size diode if inrush or thermal limited. |
| 117 | Output Capacitor | | | | | |
| 118 | COUT | 22 | | 22 | uF | Minimum value of Output capacitance |
| 119 | VO_RIPPLE_EXPECTED | | | 9.2 | V | Expected ripple voltage on Output with selected Output capacitor |
| 120 | T_HOLDUP_EXPECTED | | | 26.3 | ms | Expected holdup time with selected Output capacitor |
| 121 | ESR_LF | | Warning | 4.23 | ohms | Low frequency ESR must be between 0.01 and 3 ohms |
| 122 | ESR_HF | | Warning | 1.69 | ohms | High frequency ESR must be between 0.01 and 1 ohms |
| 123 | IC_RMS_LF | | | 0.09 | A | Low Frequency Capacitor RMS current |
| 124 | IC_RMS_HF | | | 0.28 | A | High Frequency Capacitor RMS current |
| 125 | CO_LF_LOSS | | | 0.038 | W | Estimated Low Frequency ESR loss in Output capacitor |
| 126 | CO_HF_LOSS | | | 0.133 | W | Estimated High frequency ESR loss in Output capacitor |
| 127 | Total CO LOSS | | | 0.170 | W | Total estimated losses in Output Capacitor |
| 130 | Input Bridge (BR1) and Fuse (F1) | | | | | |
| 131 | I ² t Rating | | | 3.61 | A ² *s | Minimum I ² t rating for fuse |
| 132 | Fuse Current rating | | | 0.95 | A | Minimum Current rating of fuse |
| 133 | VF | | | 0.90 | V | Input bridge Diode forward Diode drop |
| 134 | Iavg | | | 0.59 | A | Input average current at VBROWNOUT. |
| 135 | PIV_INPUT BRIDGE | | | 392 | V | Peak inverse voltage of input bridge |
| 136 | PCOND_LOSS_BRIDGE | | | 0.902 | W | Estimated Bridge Diode conduction loss |
| 137 | CIN | | | 0.22 | uF | Input capacitor. Use metallized polypropylene or film foil type with high ripple current rating |
| 138 | CIN_DF | | | 0.001 | | Input Capacitor Dissipation Factor (tan Delta) |
| 139 | CIN_PLOSS | | | 0.002 | W | Input Capacitor Loss |
| 140 | RT1 | | | 9.79 | ohms | Input Thermistor value |
| 141 | D_Precharge | | | 1N5407 | | Recommended precharge Diode |
| 144 | PFS4 small signal components | | | | | |
| 145 | C_REF | | | 1.0 | uF | REF pin capacitor value |
| 146 | RV1 | | | 4.0 | MOhms | Line sense resistor 1 |
| 147 | RV2 | | | 6.0 | MOhms | Line sense resistor 2 |
| 148 | RV3 | | | 6.0 | MOhms | Typical value of the lower resistor connected to the V-PIN. Use 1% resistor only! |
| 149 | RV4 | | | 151.7 | kOhms | Description pending, could be modified based on feedback chain R1-R4 |
| 150 | C_V | | | 0.527 | nF | V pin decoupling capacitor (RV4 and C_V should have a time constant of 80us) Pick the closest available capacitance. |
| 151 | C_VCC | | | 1.0 | uF | Supply decoupling capacitor |
| 152 | C_C | | | 100 | nF | Feedback C pin decoupling capacitor |
| 153 | Power good Vo lower threshold VPG(L) | | | 333 | V | Vo lower threshold voltage at which power good signal will trigger |
| 154 | PGT set resistor | | | 312.7 | kohm | Power good threshold setting resistor |



| 157 Feedback Components | | | | | | |
|---|--|--|--|----------|-------|---|
| 158 | RFB_1 | | | 4.00 | Mohms | Feedback network, first high voltage divider resistor |
| 159 | RFB_2 | | | 6.00 | Mohms | Feedback network, second high voltage divider resistor |
| 160 | RFB_3 | | | 6.00 | Mohms | Feedback network, third high voltage divider resistor |
| 161 | RFB_4 | | | 151.7 | kohms | Feedback network, lower divider resistor |
| 162 | CFB_1 | | | 0.527 | nF | Feedback network, loop speedup capacitor. (R4 and C1 should have a time constant of 80us) Pick the closest available capacitance. |
| 163 | RFB_5 | | | 38.3 | kohms | Feedback network: zero setting resistor |
| 164 | CFB_2 | | | 1000 | nF | Feedback component- noise suppression capacitor |
| 167 Loss Budget (Estimated at VACMIN) | | | | | | |
| 168 | PFS Losses | | | 1.464 | W | Total estimated losses in PFS |
| 169 | Boost diode Losses | | | 0.471 | W | Total estimated losses in Output Diode |
| 170 | Input Bridge losses | | | 0.902 | W | Total estimated losses in input bridge module |
| 171 | Input Capacitor Losses | | | 0.002 | W | Total estimated losses in input capacitor |
| 172 | Inductor losses | | | 9.514 | W | Total estimated losses in PFC choke |
| 173 | Output Capacitor Loss | | | 0.170 | W | Total estimated losses in Output capacitor |
| 174 | EMI choke copper loss | | | 0.031 | W | Total estimated losses in EMI choke copper |
| 175 | Total losses | | | 12.555 | W | Overall loss estimate |
| 176 | Efficiency | | | 0.81 | | Estimated efficiency at VACMIN, full load. |
| 179 CAPZero component selection recommendation | | | | | | |
| 180 | CAPZero Device | | | CAP200DG | | (Optional) Recommended CAPZero device to discharge X-Capacitor with time constant of 1 second |
| 181 | Total Series Resistance (Rcapzero1+Rcapzero2) | | | 1.046 | MOhms | Maximum Total Series resistor value to discharge X-Capacitors |
| 184 EMI filter components recommendation | | | | | | |
| 185 | CX2 | | | 330 | nF | X capacitor after differential mode choke and before bridge, ratio with Po |
| 186 | LDM_calc | | | 461 | uH | Estimated minimum differential inductance to avoid <10kHz resonance in input current |
| 187 | CX1 | | | 330 | nF | X capacitor before common mode choke, ratio with Po |
| 188 | LCM | | | 10.0 | mH | typical common mode choke value |
| 189 | LCM_leakage | | | 30 | uH | estimated leakage inductance of CM choke, typical from 30~60uH |
| 190 | CY1 (and CY2) | | | 220 | pF | typical Y capacitance for common mode noise suppression |
| 191 | LDM_Actual | | | 431 | uH | cal_LDM minus LCM_leakage, utilizing CM leakage inductance as DM choke. |
| 192 | DCR_LCM | | | 0.070 | Ohms | Total DCR of CM choke for estimating copper loss |
| 193 | DCR_LDM | | | 0.030 | Ohms | Total DCR of DM choke(or CM #2) for estimating copper loss |
| 195 | Note: CX2 can be placed between CM chock and DM choke depending on EMI design requirement. | | | | | |

Note: All warnings/info flags were verified during optimization and actual bench test using prototype design unit.

10 Flyback DC-DC Transformer Design Spreadsheet

| 1 | DCDC_LYTSwitch6_Flyback_040419; Rev.1.0; Copyright Power Integrations 2019 | INPUT | INFO | OUTPUT | UNITS | DCDC LYTSwitch6 Flyback Design Spreadsheet |
|----|--|----------|---------|----------|----------|--|
| 2 | APPLICATION VARIABLES | | | | | Design Title |
| 3 | VDCIN_MIN | 400 | | 400 | V | Minimum input DC voltage |
| 4 | VDCIN_MAX | 420 | | 420 | V | Maximum input DC voltage |
| 5 | VOUT | 42.00 | | 42.00 | V | Output voltage |
| 6 | IOUT | 1.200 | | 1.200 | A | Output current |
| 7 | POUT | | | 50.40 | W | Output power |
| 8 | EFFICIENCY | 0.94 | | 0.94 | | DC-DC efficiency estimate at full load |
| 9 | FACTOR_Z | | | 0.50 | | Z-factor estimate |
| 10 | ENCLOSURE | ADAPTER | | ADAPTER | | Power supply enclosure |
| 11 | | | | | | |
| 12 | PRIMARY CONTROLLER SELECTION | | | | | |
| 13 | ILIMIT_MODE | STANDARD | | STANDARD | | Device current limit mode |
| 14 | VDRAIN_BREAKDOWN | 650 | | 650 | V | Device breakdown voltage |
| 15 | DEVICE_GENERIC | AUTO | | LYT60X7 | | Generic device code |
| 16 | DEVICE_CODE | | | LYT6067C | | Actual device code |
| 17 | POUT_MAX | | | 60 | W | Power capability of the device based on thermal performance |
| 18 | RDSON_100DEG | | | 1.82 | Ω | Primary switch on time drain resistance at 100 degC |
| 19 | ILIMIT_MIN | | | 1.348 | A | Minimum current limit of the primary switch |
| 20 | ILIMIT_TYP | | | 1.450 | A | Typical current limit of the primary switch |
| 21 | ILIMIT_MAX | | | 1.552 | A | Maximum current limit of the primary switch |
| 22 | VDRAIN_ON_PRSW | | | 0.24 | V | Primary switch on time drain voltage |
| 23 | VDRAIN_OFF_PRSW | | Warning | 600.0 | V | The peak drain voltage on the switch is higher than 585V : Decrease the device VOR |
| 25 | WORST CASE ELECTRICAL PARAMETERS | | | | | |
| 26 | FSWITCHING_MAX | 74000 | | 74000 | Hz | Maximum switching frequency at full load and minimum DC input voltage |
| 27 | VOR | | | 110.0 | V | Secondary voltage reflected to the primary when the primary switch turns off |
| 28 | KP | | | 1.09 | | Measure of continuous/discontinuous mode of operation |
| 29 | MODE_OPERATION | | | DCM | | Mode of operation |
| 30 | DUTYCYCLE | | | 0.202 | | Primary switch duty cycle |
| 31 | TIME_ON | | | 3.28 | us | Primary switch on-time |
| 32 | TIME_OFF | | | 10.82 | us | Primary switch off-time |
| 33 | LPRIMARY_MIN | | | 827.7 | uH | Minimum primary inductance |
| 34 | LPRIMARY_TYP | 871 | | 871.3 | uH | Typical primary inductance |
| 35 | LPRIMARY_TOL | | | 5.0 | % | Primary inductance tolerance |
| 36 | LPRIMARY_MAX | | | 914.9 | uH | Maximum primary inductance |



| | | | | | | |
|----|--|---------|------|-----------------|-----------------------|---|
| 38 | PRIMARY CURRENTS | | | | | |
| 39 | IPEAK_PRIMARY | | | 1.452 | A | Primary switch peak current |
| 40 | IPEDESTAL_PRIMARY | | | 0.000 | A | Primary switch current pedestal |
| 41 | IAVG_PRIMARY | | | 0.130 | A | Primary switch average current |
| 42 | IRIPPLE_PRIMARY | | | 1.452 | A | Primary switch ripple current |
| 43 | IRMS_PRIMARY | | | 0.355 | A | Primary switch RMS current |
| 45 | SECONDARY CURRENTS | | | | | |
| 46 | IPEAK_SECONDARY | | | 3.811 | A | Secondary winding peak current |
| 47 | IPEDESTAL_SECONDARY | | | 0.000 | A | Secondary winding current pedestal |
| 48 | IRMS_SECONDARY | | | 1.776 | A | Secondary winding RMS current |
| 49 | IRIPPLE_CAP_OUT | | | | | |
| 50 | | | | | | |
| 51 | TRANSFORMER CONSTRUCTION PARAMETERS | | | | | |
| 52 | CORE SELECTION | | | | | |
| 53 | CORE | PQ20/20 | Info | PQ20/20 | | The transformer windings may not fit: pick a bigger core or bobbin and refer to the Transformer Parameters tab for fit calculations |
| 54 | CORE CODE | | | B65875A0000R095 | | Core code |
| 55 | AE | | | 62.90 | mm ² | Core cross sectional area |
| 56 | LE | | | 45.20 | mm | Core magnetic path length |
| 57 | AL | | | 3300 | nH/turns ² | Ungapped core effective inductance |
| 58 | VE | | | 2843.0 | mm ³ | Core volume |
| 59 | BOBBIN | | | B65876E1014D001 | | Bobbin |
| 60 | AW | | | 35.00 | mm ² | Window area of the bobbin |
| 61 | BW | | | 11.70 | mm | Bobbin width |
| 62 | MARGIN | | | 0.0 | mm | Safety margin width (Half the primary to secondary creepage distance) |
| 64 | PRIMARY WINDING | | | | | |
| 65 | NPRIMARY | | | 63 | | Primary turns |
| 66 | BPEAK | | | 3667 | Gauss | Peak flux density |
| 67 | BMAX | | | 3308 | Gauss | Maximum flux density |
| 68 | BAC | | | 1654 | Gauss | AC flux density (0.5 x Peak to Peak) |
| 69 | ALG | | | 220 | nH/turns ² | Typical gapped core effective inductance |
| 70 | LG | | | 0.336 | mm | Core gap length |
| 71 | LAYERS_PRIMARY | | | 2 | | Number of primary layers |
| 72 | AWG_PRIMARY | | | 29 | AWG | Primary winding wire AWG |
| 73 | OD_PRIMARY_INSULATED | | | 0.337 | mm | Primary winding wire outer diameter with insulation |
| 74 | OD_PRIMARY_BARE | | | 0.286 | mm | Primary winding wire outer diameter without insulation |
| 75 | CMA_PRIMARY | | | 357 | Cmil/A | Primary winding wire CMA |
| 77 | PRIMARY BIAS WINDING | | | | | |
| 78 | NBIAS_PRIMARY | | | 9 | | Primary bias turns |
| 80 | SECONDARY WINDING | | | | | |
| 81 | NSECONDARY | | | 24 | | Secondary turns |

| | | | | | | |
|-----|-------------------------------------|------|---------|----------|--------|--|
| 82 | AWG_SECONDARY | 23 | | 23 | AWG | Secondary winding wire AWG |
| 83 | OD_SECONDARY_INSULATED | | | 0.879 | mm | Secondary winding wire outer diameter with insulation |
| 84 | OD_SECONDARY_BARE | | | 0.573 | mm | Secondary winding wire outer diameter without insulation |
| 85 | CMA_SECONDARY | | | 287 | Cmil/A | Secondary winding wire CMA |
| 87 | SECONDARY BIAS WINDING | | | | | |
| 88 | NBIAS_SECONDARY | | | 10 | | Secondary bias turns (Required only for VOUT>24V or VOUT<4.4V) |
| 90 | PRIMARY COMPONENTS SELECTION | | | | | |
| 91 | LINE UNDERVOLTAGE | | | | | |
| 92 | OV REQUIRED | | | 428.4 | V | Required DC over-voltage threshold |
| 93 | OV ACTUAL | | Warning | 430.2 | V | The device voltage stress will be higher than 90% of the device BVDS when overvoltage is triggered |
| 94 | RLS | | | 3.64 | MΩ | Connect two 1.82 MΩ resistors to the V-pin for the required UV/OV threshold |
| 95 | BROWN-IN ACTUAL | | | 103.2 | V | Actual DC brown-in threshold |
| 96 | BROWN-OUT ACTUAL | | | 93.4 | V | Actual DC brown-out threshold |
| 99 | PRIMARY BIAS WINDING DIODE | | | | | |
| 100 | VBIAS_PRIMARY | | | 15.0 | V | Rectified bias voltage |
| 101 | VF_BIAS_PRIMARY | | | 0.70 | V | Secondary bias winding diode forward drop |
| 102 | VREVERSE_PRIBIASDIODE_PRIMARY | | | 75.00 | V | Primary bias diode reverse voltage (not accounting parasitic voltage ring) |
| 103 | CBIAS_PRIMARY | | | 22 | μF | Primary bias winding rectification capacitor |
| 104 | CBPP | | | 0.47 | μF | BPP pin capacitor |
| 106 | SECONDARY COMPONENTS | | | | | |
| 107 | FEEDBACK | | | | | |
| 108 | RFB_UPPER | | | 100.00 | kΩ | Upper feedback resistor (connected to the first output voltage) |
| 109 | RFB_LOWER | | | 3.09 | kΩ | Lower feedback resistor |
| 110 | CFB_LOWER | | | 330 | pF | Lower feedback resistor decoupling capacitor |
| 112 | RECTIFIER | | | | | |
| 113 | VREVERSE_RECTIFIER | | | 202.0 | | Secondary rectifier reverse voltage (not accounting parasitic voltage ring) |
| 114 | TYPE_RECTIFIER | AUTO | | DIODE | | Type of secondary rectifier used |
| 115 | RECTIFIER | AUTO | | STTH3R04 | | Secondary rectifier |
| 116 | VF_RECTIFIER | | | 1.500 | | Secondary rectifier forward voltage drop |
| 117 | BVDSS_RECTIFIER | | | 400 | | Breakdown voltage of the secondary rectifier |
| 118 | RDSON_RECTIFIER | | | NA | | On-time drain to source resistance of the secondary rectifier |
| 119 | TRR_RECTIFIER | | | 18.0 | | Reverse recovery time of |



| | | | | | | the ultra-fast diode |
|------------|-------------------------------------|-----|--|-------|-------|---|
| 121 | SECONDARY BIAS WINDING DIODE | | | | | |
| 122 | VBIAS_SECONDARY | 16 | | 16 | V | Rectified secondary bias voltage |
| 123 | VF_BIAS_SECONDARY | | | 0.7 | V | Secondary bias winding diode forward drop |
| 124 | VREVERSE_BIASDIODE_SECONDARY | | | 82.67 | V | Secondary bias diode reverse voltage (not accounting parasitic voltage ring) |
| 125 | CBIAS_SECONDARY | | | 22 | uF | Secondary bias winding rectification capacitor |
| 127 | TOLERANCE ANALYSIS | | | | | |
| 128 | USER_VDC | | | 410 | V | Input DC voltage corner to be evaluated |
| 129 | USER_ILIMIT | TYP | | 1.450 | A | Current limit corner to be evaluated |
| 130 | USER_LPRIMARY | TYP | | 871.3 | uH | Primary inductance corner to be evaluated |
| 131 | MODE_OPERATION | | | DCM | | Mode of operation |
| 132 | KP | | | 1.181 | | Measure of continuous/discontinuous mode of operation |
| 133 | FSWITCHING | | | 63528 | Hz | Switching frequency at full load and valley of the rectified minimum AC input voltage |
| 134 | DUTYCYCLE | | | 0.185 | | Steady state duty cycle |
| 135 | TIME_ON | | | 2.91 | us | Primary switch on-time |
| 136 | TIME_OFF | | | 12.83 | us | Primary switch off-time |
| 137 | IPEAK_PRIMARY | | | 1.371 | A | Primary switch peak current |
| 138 | IPEDESTAL_PRIMARY | | | 0.000 | A | Primary switch current pedestal |
| 139 | IAVERAGE_PRIMARY | | | 0.127 | A | Primary switch average current |
| 140 | IRIPPLE_PRIMARY | | | 1.371 | A | Primary switch ripple current |
| 141 | IRMS_PRIMARY | | | 0.341 | A | Primary switch RMS current |
| 142 | BPEAK | | | 3263 | Gauss | Peak flux density |
| 143 | BMAX | | | 3014 | Gauss | Maximum flux density |
| 144 | BAC | | | 1507 | Gauss | AC flux density (0.5 x Peak to Peak) |

Note: All warnings/info flags were verified during optimization and actual bench test using prototype design unit.

11 Performance Data

All measurements were performed at room temperature using E-load and 36 V actual LED panel load.

11.1 CV/CC Output Characteristic Curve

CC regulation was measured using E-load at CR load.

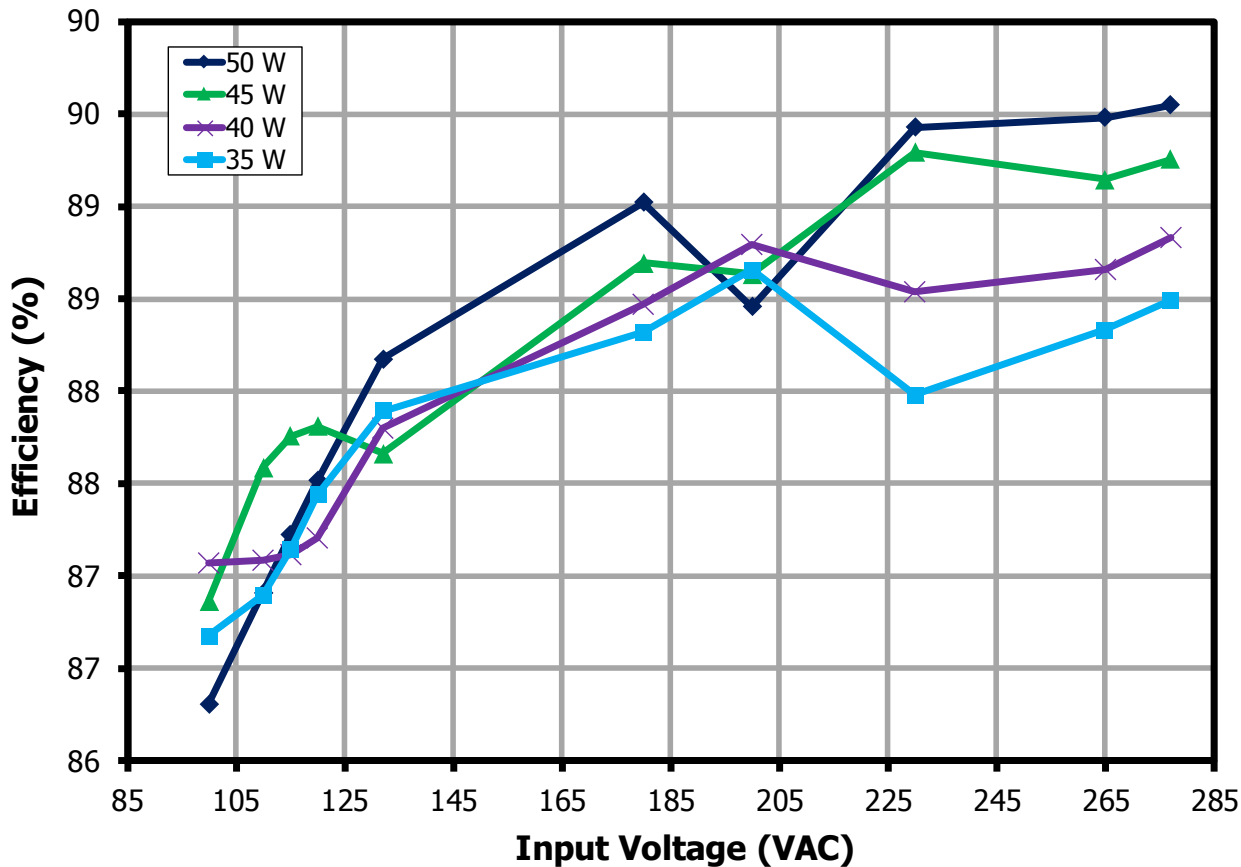


Figure 21 – CV/CC Curve.

11.2 System Efficiency

Efficiency is above 86% throughout the input voltage range.

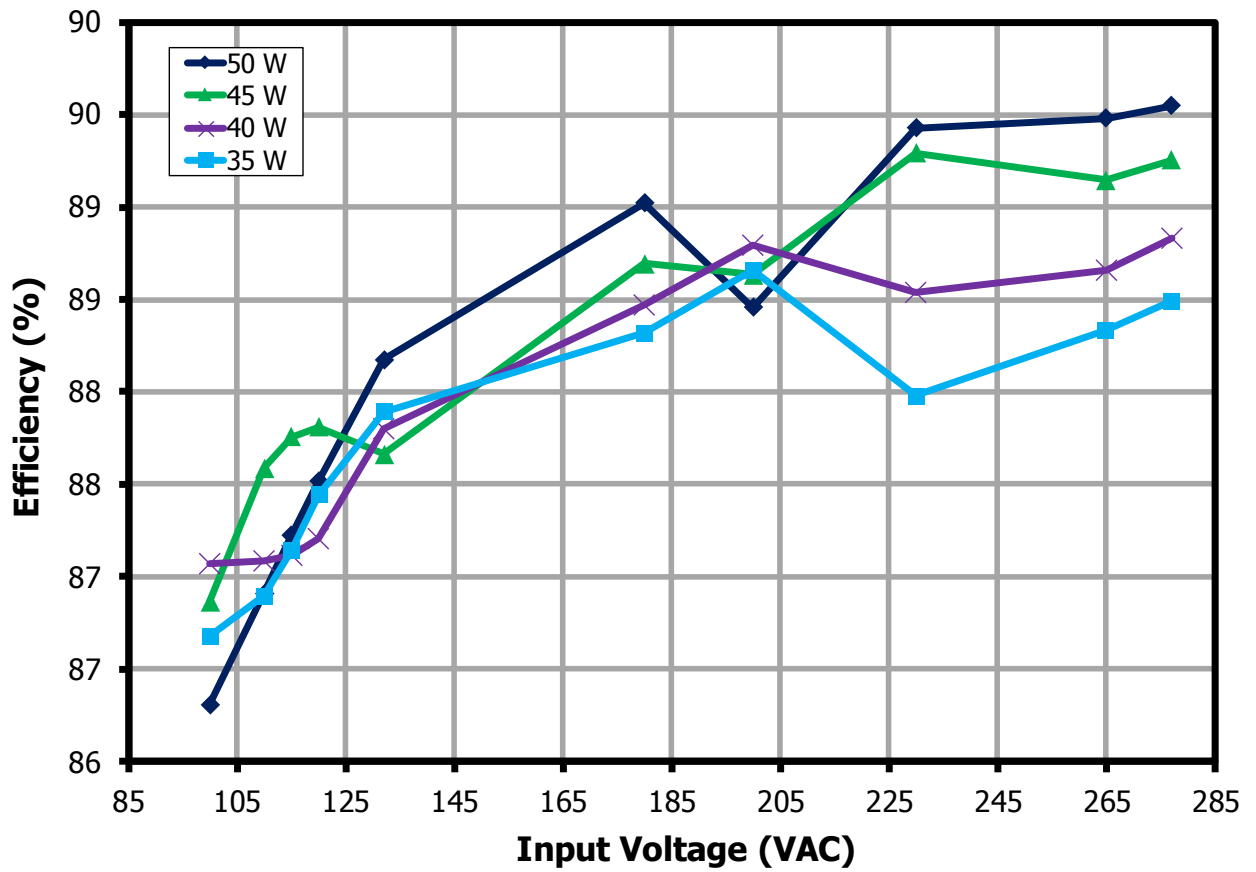


Figure 22 – Efficiency vs. Line and 36 V LED Panel Load.



11.3 **Line Regulation Power Selection**

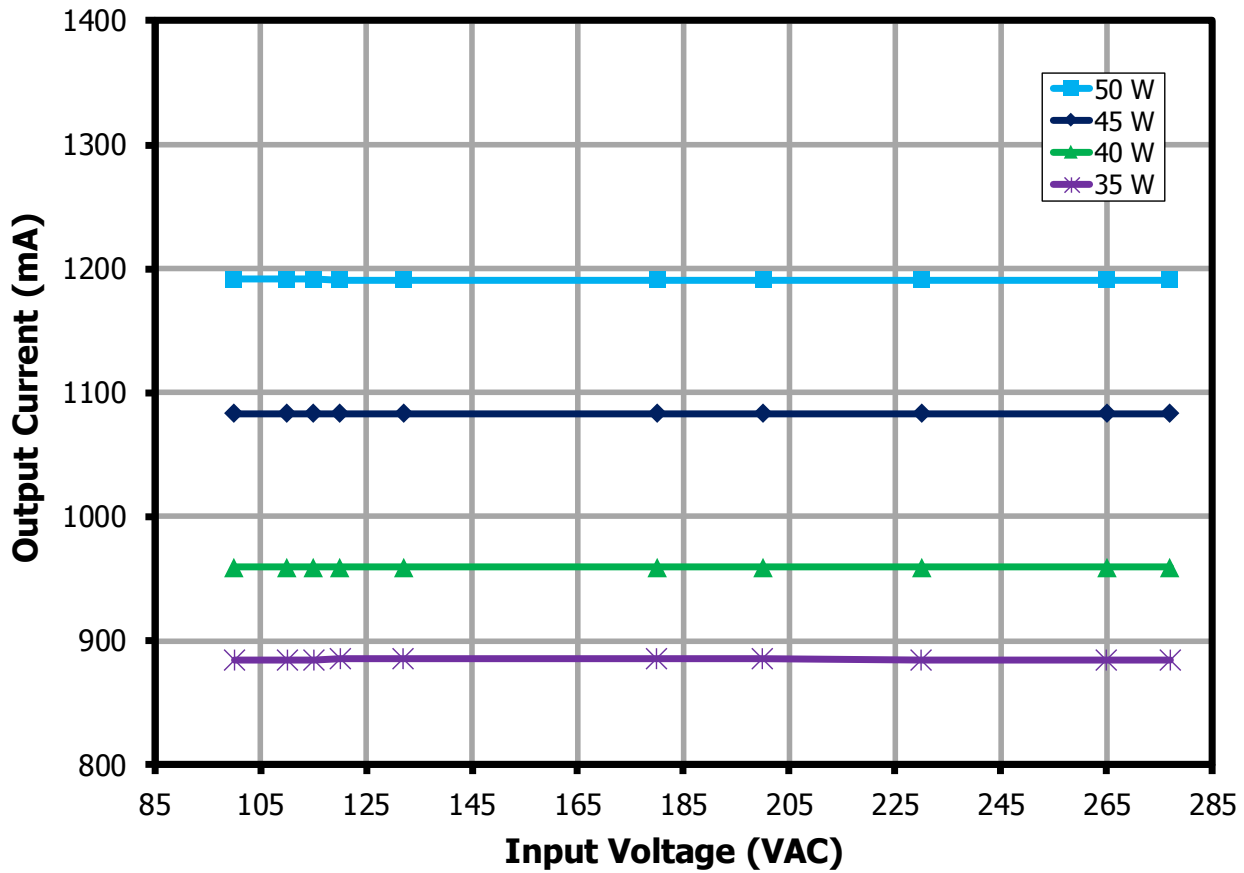


Figure 23 – Current Regulation vs. Line and 36 V LED Panel Load.

11.4 **Power Factor**

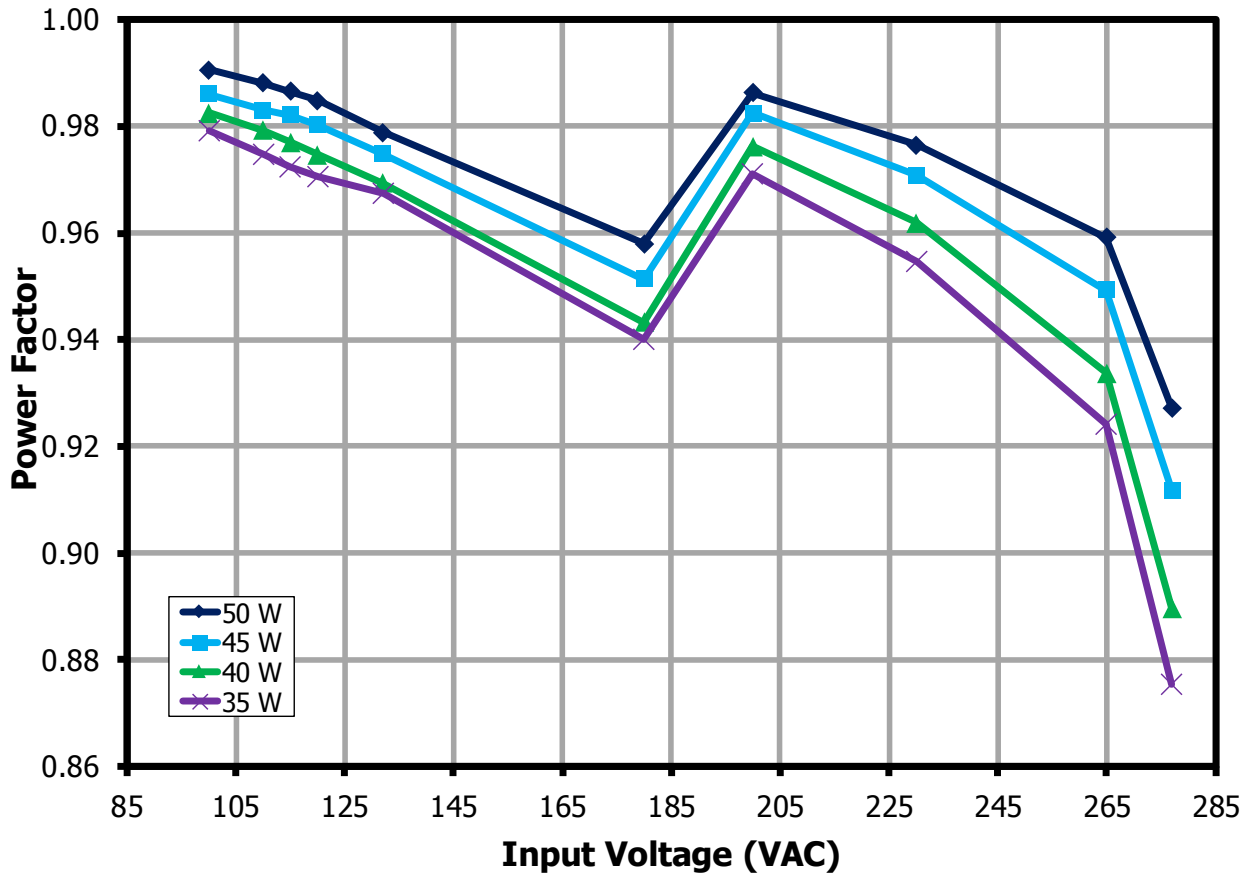


Figure 24 – Power Factor vs. Line and 36 V LED Panel Load.



11.5 %ATHD

%ATHD is less than 20% throughout all the input voltage range.

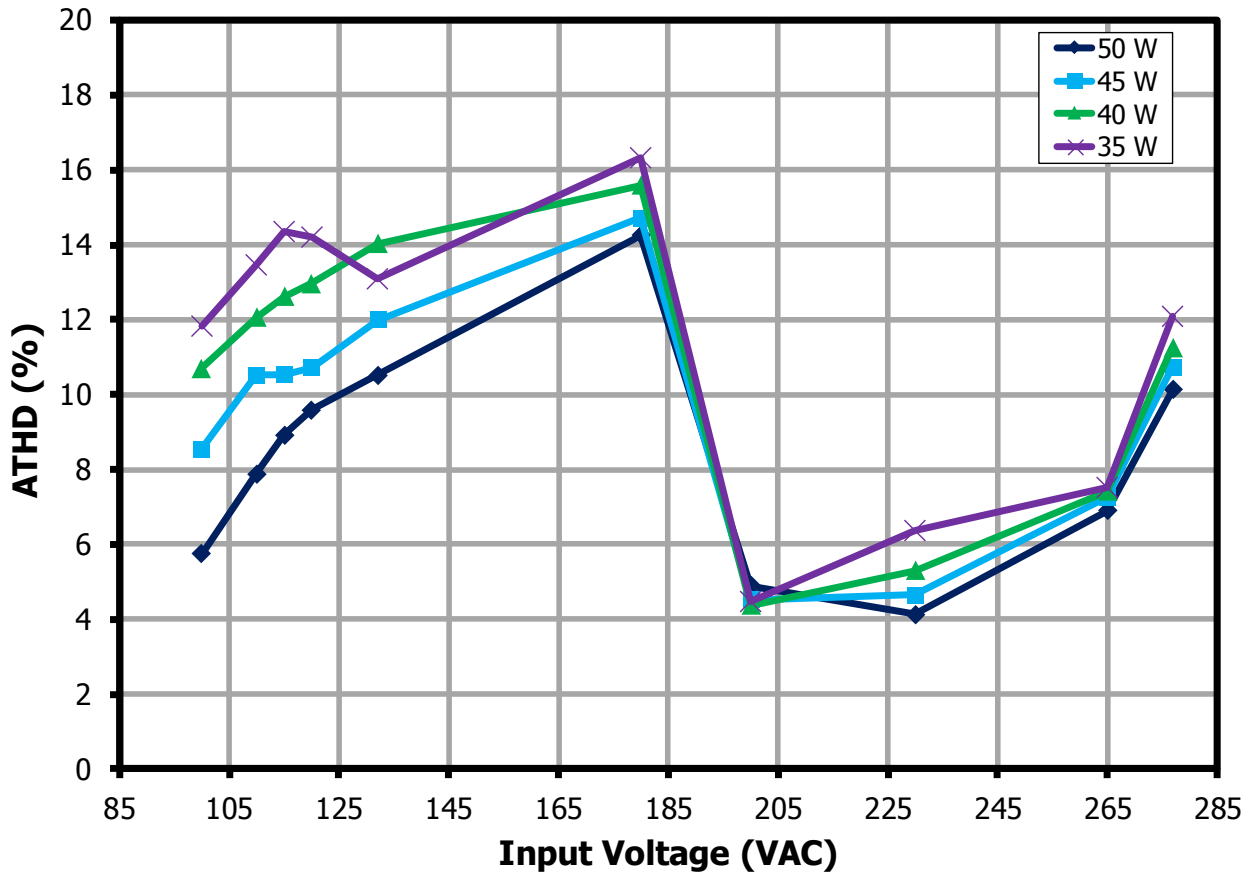


Figure 25 – %ATHD vs. Line and 36 V LED Panel Load.

11.6 Individual Harmonic Content at 50 W Power Selection

Current harmonic content is well below the Class C limit.

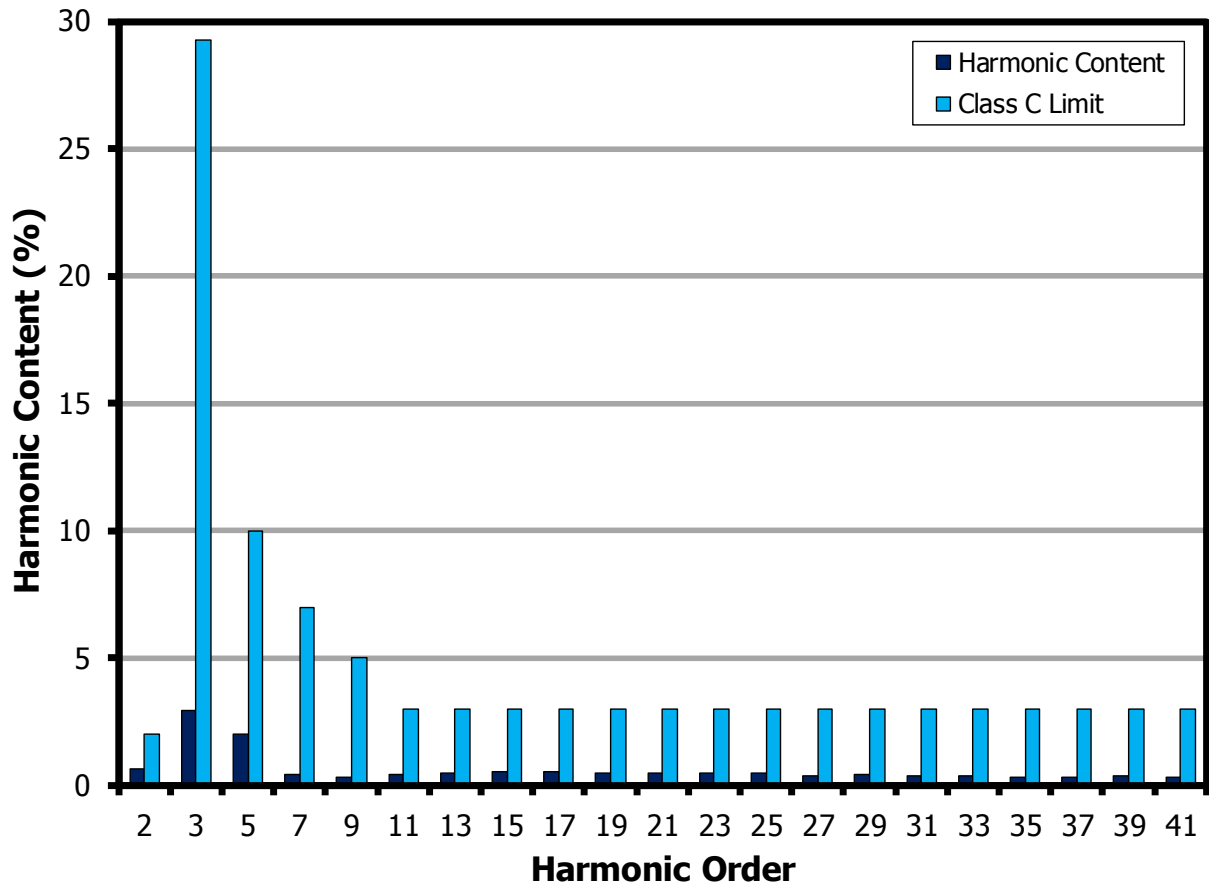


Figure 26 – 36 V LED Load Panel Input Current Harmonics at 230 VAC, 50 Hz.



11.7 **Individual Harmonic Content at 35 W Power Selection**

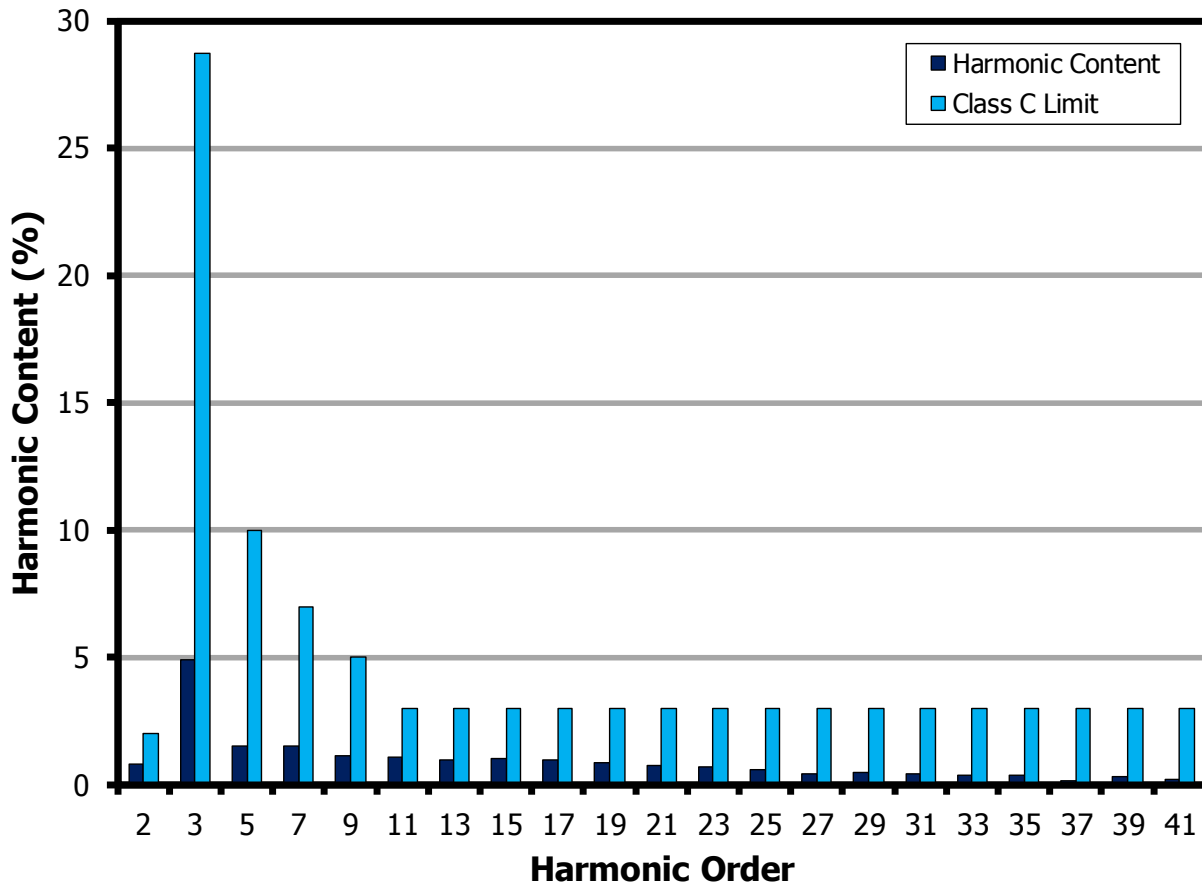


Figure 27 – 36 V LED Load Panel Input Current Harmonics at 230 VAC, 50 Hz.

11.8 **No-Load Input Power**

Integration time: 5 minutes

No Load input power is less than 200 mW.

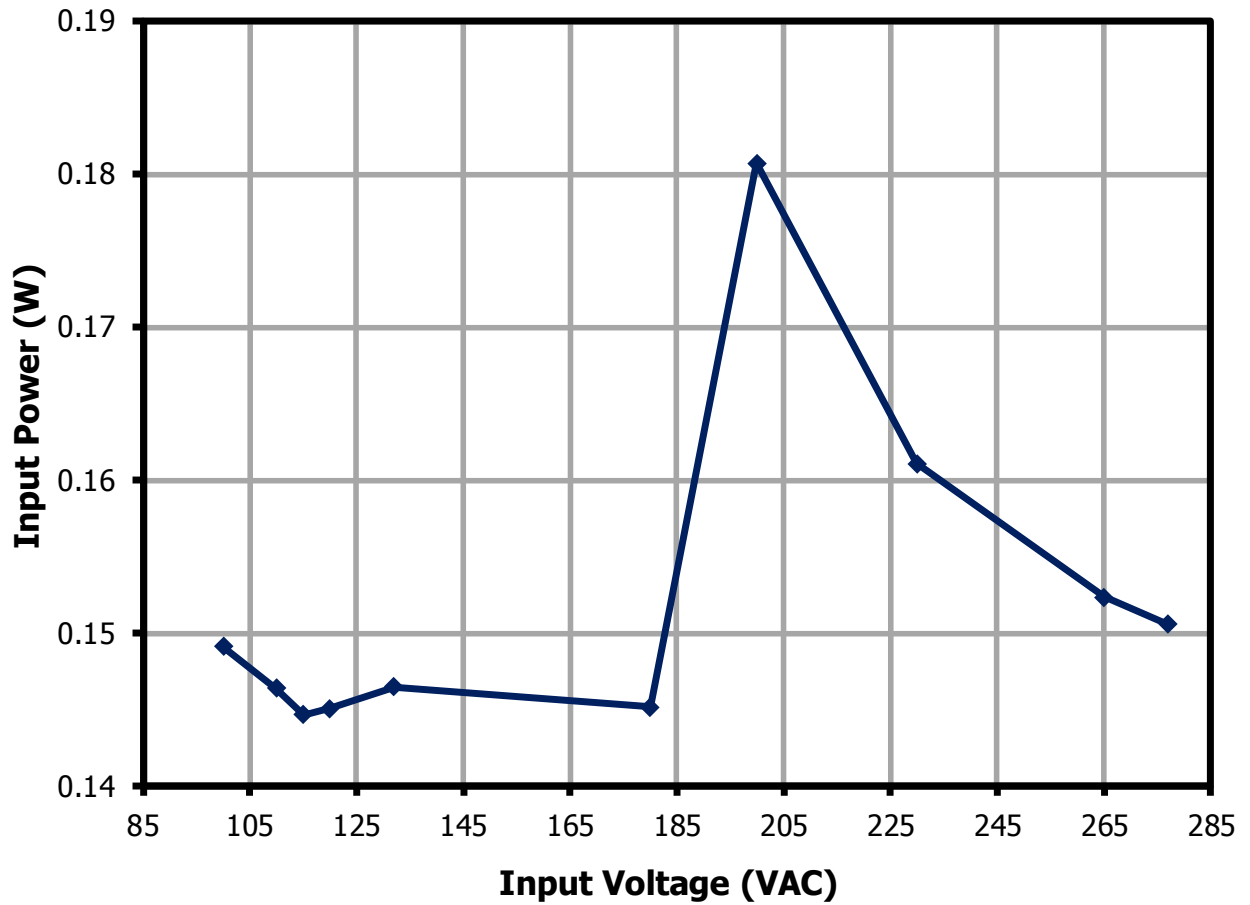


Figure 28 – No-Load Input Power vs. Line.



12 Test Data

12.1 1200 mA

| Input | | Input Measurement | | | | | LED Load Measurement | | | Efficiency (%) |
|-------------------------|-----------|-------------------------------------|--------------------------------------|---------------------|------|--------|-------------------------------------|--------------------------------------|----------------------|----------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | % ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | |
| 100 | 60 | 100 | 488.37 | 48.34 | 0.99 | 5.75 | 35.01 | 1191.50 | 41.72 | 86.31 |
| 110 | 60 | 110 | 441.87 | 48.00 | 0.99 | 7.89 | 35.01 | 1191.50 | 41.72 | 86.91 |
| 115 | 60 | 115 | 421.74 | 47.81 | 0.99 | 8.93 | 35.01 | 1191.30 | 41.71 | 87.23 |
| 120 | 60 | 120 | 403.27 | 47.65 | 0.98 | 9.60 | 35.01 | 1191.20 | 41.70 | 87.52 |
| 132 | 60 | 132 | 366.05 | 47.29 | 0.98 | 10.52 | 35.01 | 1191.10 | 41.70 | 88.18 |
| 180 | 50 | 180 | 271.56 | 46.84 | 0.96 | 14.26 | 35.01 | 1191.00 | 41.69 | 89.02 |
| 200 | 50 | 200 | 238.96 | 47.13 | 0.99 | 4.89 | 35.00 | 1191.00 | 41.69 | 88.46 |
| 230 | 50 | 230 | 207.47 | 46.61 | 0.98 | 4.14 | 35.00 | 1190.80 | 41.68 | 89.43 |
| 265 | 50 | 265 | 183.26 | 46.58 | 0.96 | 6.89 | 35.00 | 1190.80 | 41.68 | 89.48 |
| 277 | 60 | 277 | 181.20 | 46.55 | 0.93 | 10.12 | 35.00 | 1190.90 | 41.69 | 89.55 |

12.2 1100 mA

| Input | | Input Measurement | | | | | LED Load Measurement | | | Efficiency (%) |
|-------------------------|-----------|-------------------------------------|--------------------------------------|---------------------|------|--------|-------------------------------------|--------------------------------------|----------------------|----------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | % ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | |
| 100 | 60 | 100 | 439.65 | 43.33 | 0.99 | 8.55 | 34.74 | 1083.50 | 37.64 | 86.86 |
| 110 | 60 | 110 | 397.41 | 42.96 | 0.98 | 10.52 | 34.73 | 1083.40 | 37.63 | 87.59 |
| 115 | 60 | 115 | 379.81 | 42.88 | 0.98 | 10.54 | 34.73 | 1083.30 | 37.63 | 87.76 |
| 120 | 60 | 120 | 364.28 | 42.85 | 0.98 | 10.72 | 34.73 | 1083.30 | 37.63 | 87.81 |
| 132 | 60 | 132 | 333.59 | 42.92 | 0.97 | 12.00 | 34.73 | 1083.20 | 37.62 | 87.66 |
| 180 | 50 | 180 | 247.59 | 42.41 | 0.95 | 14.71 | 34.73 | 1083.00 | 37.62 | 88.69 |
| 200 | 50 | 200 | 215.98 | 42.44 | 0.98 | 4.52 | 34.73 | 1083.10 | 37.62 | 88.63 |
| 230 | 50 | 230 | 188.62 | 42.13 | 0.97 | 4.65 | 34.73 | 1083.10 | 37.62 | 89.29 |
| 265 | 50 | 265 | 167.74 | 42.20 | 0.95 | 7.26 | 34.73 | 1083.20 | 37.62 | 89.14 |
| 277 | 60 | 277 | 166.80 | 42.15 | 0.91 | 10.73 | 34.73 | 1083.20 | 37.62 | 89.25 |

12.3 960 mA

| Input | | Input Measurement | | | | | LED Load Measurement | | | Efficiency (%) |
|-------------------------|-----------|-------------------------------------|--------------------------------------|---------------------|------|--------|-------------------------------------|--------------------------------------|----------------------|----------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | % ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | |
| 100 | 60 | 100 | 386.09 | 37.92 | 0.98 | 10.71 | 34.42 | 959.20 | 33.01 | 87.07 |
| 110 | 60 | 110 | 352.03 | 37.91 | 0.98 | 12.06 | 34.42 | 959.20 | 33.01 | 87.09 |
| 115 | 60 | 115 | 337.39 | 37.89 | 0.98 | 12.62 | 34.42 | 959.10 | 33.01 | 87.11 |
| 120 | 60 | 120 | 323.58 | 37.85 | 0.97 | 12.97 | 34.42 | 959.10 | 33.01 | 87.21 |
| 132 | 60 | 132 | 293.82 | 37.60 | 0.97 | 14.04 | 34.42 | 959.10 | 33.01 | 87.80 |
| 180 | 50 | 180 | 219.69 | 37.31 | 0.94 | 15.60 | 34.42 | 959.10 | 33.01 | 88.47 |
| 200 | 50 | 200 | 190.37 | 37.17 | 0.98 | 4.37 | 34.42 | 959.00 | 33.01 | 88.79 |
| 230 | 50 | 230 | 168.44 | 37.28 | 0.96 | 5.30 | 34.42 | 959.10 | 33.01 | 88.54 |
| 265 | 50 | 265 | 150.42 | 37.23 | 0.93 | 7.42 | 34.42 | 959.10 | 33.01 | 88.66 |
| 277 | 60 | 277 | 150.72 | 37.16 | 0.89 | 11.27 | 34.42 | 959.10 | 33.01 | 88.83 |



12.4 **850 mA**

| Input | | Input Measurement | | | | | LED Load Measurement | | | Efficiency (%) |
|-------------------------|-----------|-------------------------------------|--------------------------------------|---------------------|------|--------|-------------------------------------|--------------------------------------|----------------------|----------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | PF | % ATHD | V _{OUT} (V _{DC}) | I _{OUT} (mA _{DC}) | P _{OUT} (W) | |
| 100 | 60 | 100 | 356.95 | 34.94 | 0.98 | 11.84 | 34.22 | 884.90 | 30.29 | 86.68 |
| 110 | 60 | 110 | 325.11 | 34.85 | 0.97 | 13.48 | 34.22 | 884.90 | 30.28 | 86.90 |
| 115 | 60 | 115 | 310.85 | 34.75 | 0.97 | 14.37 | 34.22 | 884.90 | 30.28 | 87.15 |
| 120 | 60 | 120 | 297.34 | 34.64 | 0.97 | 14.20 | 34.22 | 885.00 | 30.29 | 87.44 |
| 132 | 60 | 132 | 269.87 | 34.46 | 0.97 | 13.10 | 34.22 | 885.10 | 30.29 | 87.89 |
| 180 | 50 | 180 | 202.61 | 34.29 | 0.94 | 16.31 | 34.22 | 885.00 | 30.29 | 88.32 |
| 200 | 50 | 200 | 175.92 | 34.16 | 0.97 | 4.47 | 34.22 | 885.00 | 30.29 | 88.66 |
| 230 | 50 | 230 | 156.71 | 34.42 | 0.95 | 6.36 | 34.22 | 884.90 | 30.28 | 87.98 |
| 265 | 50 | 265 | 139.96 | 34.28 | 0.92 | 7.51 | 34.22 | 884.90 | 30.28 | 88.33 |
| 277 | 60 | 277 | 141.03 | 34.22 | 0.88 | 12.09 | 34.22 | 884.90 | 30.28 | 88.49 |

12.5 **No-Load**

| Input | | Input Measurement | | | V _{OUT} |
|----------------------------|--------------|--|---|------------------------|-------------------------|
| VAC (V _{RMS}) | Freq (Hz) | V _{IN} (V _{RMS}) | I _{IN} (mA _{RMS}) | P _{IN} (W) | V (V _{DC}) |
| 100 | 60 | 100 | 56.17 | 0.149 | 42.36 |
| 110 | 60 | 110 | 54.71 | 0.146 | 42.36 |
| 115 | 60 | 115 | 54.54 | 0.145 | 42.35 |
| 120 | 60 | 120 | 54.89 | 0.145 | 42.35 |
| 132 | 60 | 132 | 55.00 | 0.146 | 42.35 |
| 180 | 50 | 180 | 54.02 | 0.145 | 42.35 |
| 200 | 50 | 200 | 52.59 | 0.181 | 42.36 |
| 230 | 50 | 230 | 50.82 | 0.161 | 42.35 |
| 265 | 50 | 265 | 48.85 | 0.152 | 42.35 |
| 277 | 60 | 277 | 49.98 | 0.151 | 42.35 |

12.6 *Individual Harmonic Content at 50 W Power Selection*

| V_{IN} (V_{RMS}) | Freq | I_{IN} (mA_{RMS}) | P_{IN} (W) | PF | %THD |
|---------------------------|-------------------|----------------------------|--------------------------|--------------------------|----------------|
| 230 | 50 | 207.50 | 46.61 | 0.98 | 4.23 |
| Harmonic Content | | | Class C Limit | | |
| nth Order | mA Content | % Content | mA Limit <25 W | mA Limit >25 W | Remarks |
| 1 | 204.10 | | | | |
| 2 | 1.37 | 0.67 | | 2 | pass |
| 3 | 6.05 | 2.96 | 158.47 | 29.30 | pass |
| 5 | 4.07 | 1.99 | 88.56 | 10 | pass |
| 7 | 0.84 | 0.41 | 46.61 | 7 | pass |
| 9 | 0.63 | 0.31 | 23.31 | 5 | pass |
| 11 | 0.82 | 0.40 | 16.31 | 3 | pass |
| 13 | 0.95 | 0.47 | 13.80 | 3 | pass |
| 15 | 1.14 | 0.56 | 11.96 | 3 | pass |
| 17 | 1.08 | 0.53 | 10.56 | 3 | pass |
| 19 | 1.00 | 0.49 | 9.44 | 3 | pass |
| 21 | 0.94 | 0.46 | 8.55 | 3 | pass |
| 23 | 0.94 | 0.46 | 7.80 | 3 | pass |
| 25 | 0.96 | 0.47 | 7.18 | 3 | pass |
| 27 | 0.75 | 0.37 | 6.65 | 3 | pass |
| 29 | 0.90 | 0.44 | 6.19 | 3 | pass |
| 31 | 0.81 | 0.40 | 5.79 | 3 | pass |
| 33 | 0.74 | 0.36 | 5.44 | 3 | pass |
| 35 | 0.64 | 0.31 | 5.13 | 3 | pass |
| 37 | 0.70 | 0.34 | 4.85 | 3 | pass |
| 39 | 0.77 | 0.38 | 4.60 | 3 | pass |
| 41 | 0.67 | 0.33 | 4.38 | 3 | pass |

12.7 **Individual Harmonic Content at 35 W Power Selection**

| V_{IN} (V_{RMS}) | Freq | I_{IN} (mA_{RMS}) | P_{IN} (W) | PF | %THD |
|---------------------------|-------------------|----------------------------|--------------------------|--------------------------|----------------|
| 230 | 50 | 156.27 | 34.41 | 0.96 | 6.29 |
| Harmonic Content | | | Class C Limit | | |
| nth Order | mA Content | % Content | mA Limit <25 W | mA Limit >25 W | Remarks |
| 1 | 151.94 | | | | |
| 2 | 1.24 | 0.82 | | 2 | pass |
| 3 | 7.44 | 4.90 | 116.98 | 28.71 | pass |
| 5 | 2.31 | 1.52 | 65.37 | 10 | pass |
| 7 | 2.33 | 1.53 | 34.41 | 7 | pass |
| 9 | 1.77 | 1.16 | 17.20 | 5 | pass |
| 11 | 1.62 | 1.07 | 12.04 | 3 | pass |
| 13 | 1.49 | 0.98 | 10.19 | 3 | pass |
| 15 | 1.56 | 1.03 | 8.83 | 3 | pass |
| 17 | 1.52 | 1.00 | 7.79 | 3 | pass |
| 19 | 1.30 | 0.86 | 6.97 | 3 | pass |
| 21 | 1.15 | 0.76 | 6.31 | 3 | pass |
| 23 | 1.08 | 0.71 | 5.76 | 3 | pass |
| 25 | 0.92 | 0.61 | 5.30 | 3 | pass |
| 27 | 0.62 | 0.41 | 4.91 | 3 | pass |
| 29 | 0.72 | 0.47 | 4.57 | 3 | pass |
| 31 | 0.62 | 0.41 | 4.27 | 3 | pass |
| 33 | 0.55 | 0.36 | 4.01 | 3 | pass |
| 35 | 0.53 | 0.35 | 3.78 | 3 | pass |
| 37 | 0.25 | 0.16 | 3.58 | 3 | pass |
| 39 | 0.48 | 0.32 | 3.40 | 3 | pass |
| 41 | 0.30 | 0.20 | 3.23 | 3 | pass |

13 Dimming Performance

Dimming performance data were taken at room temperature using resistor dimming (0-100 kΩ).

13.1 Dimming Curve

13.1.1 0-10 kΩ Resistor Dimming

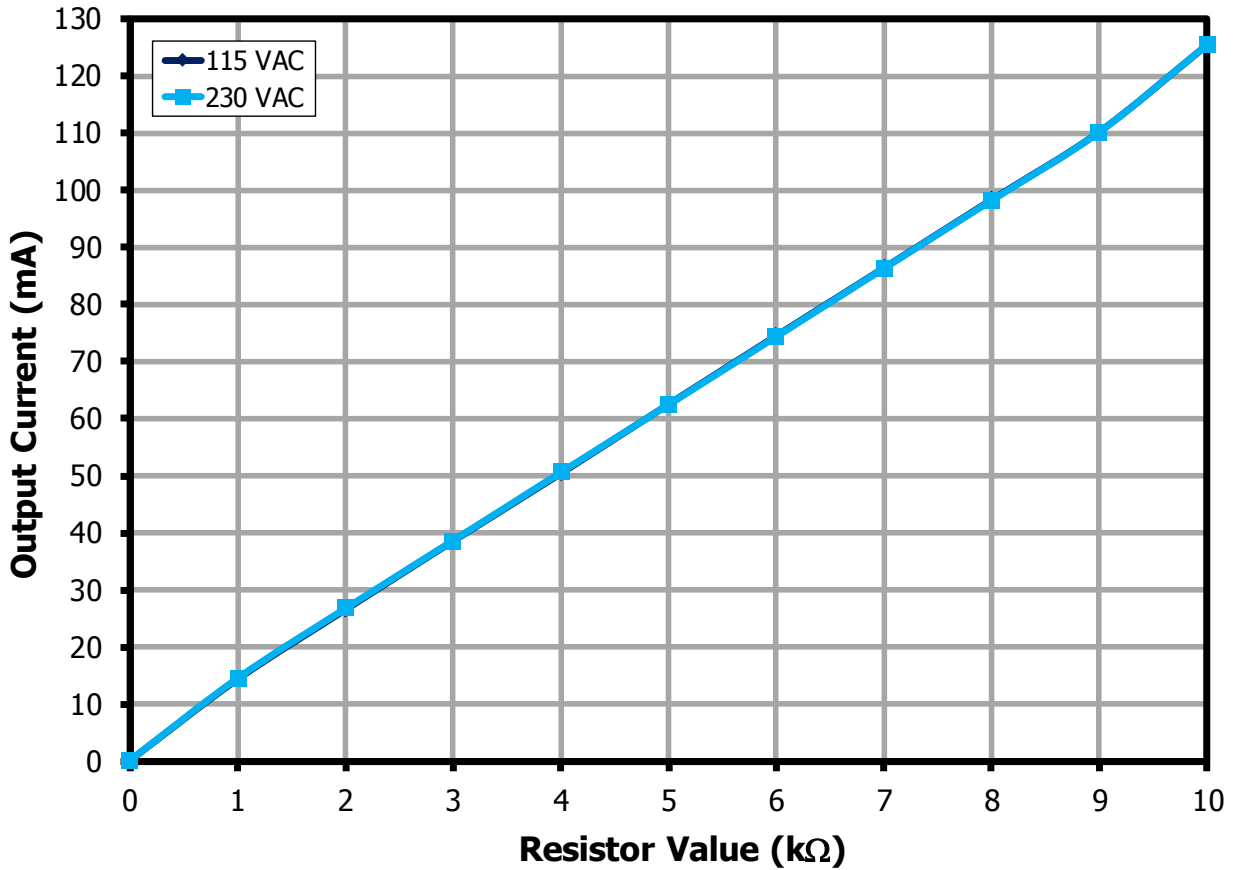


Figure 29 – 0-100 kΩ Resistor Dimming Curve at 36 V LED Load.



13.1.2 0-100 kΩ Resistor Dimming

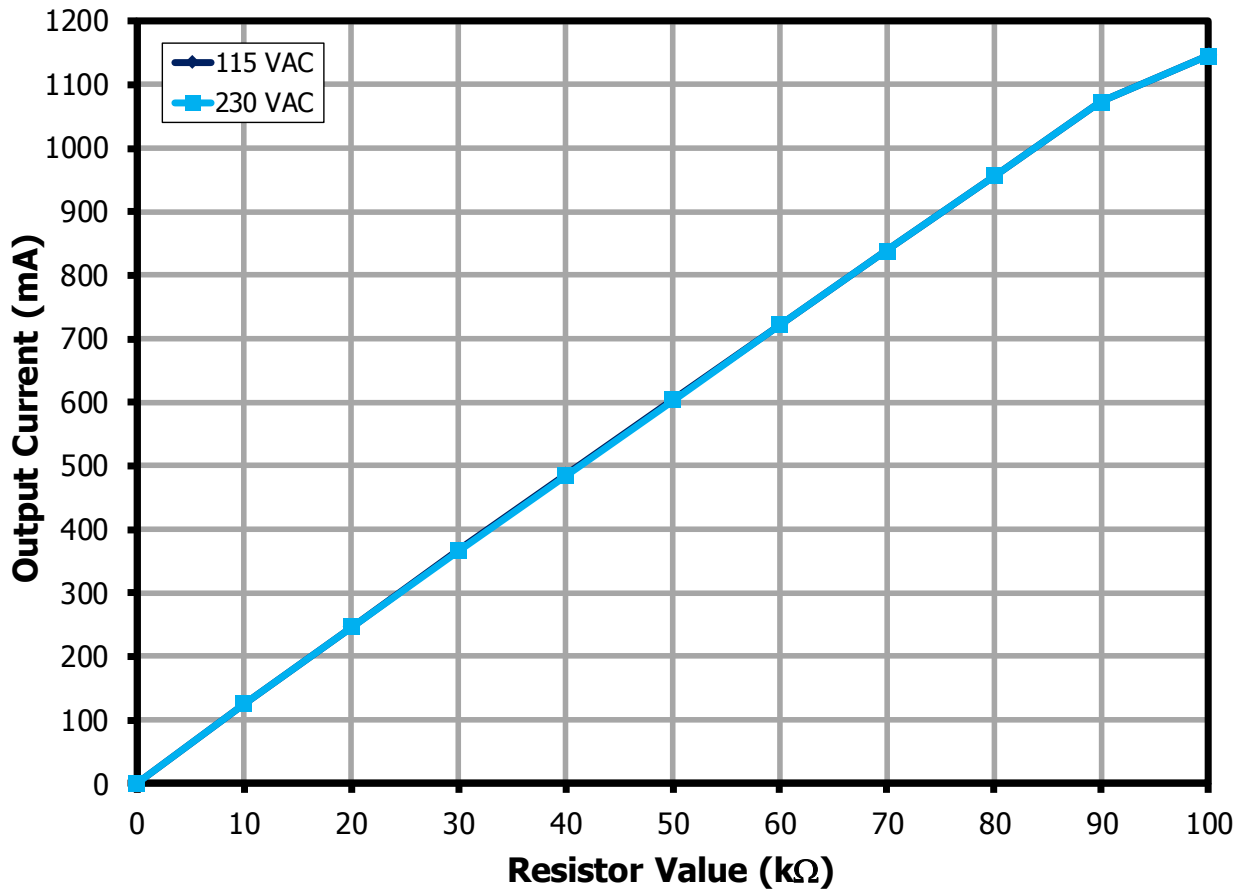


Figure 30 – 0-100 kΩ Resistor Dimming Curve at 36 V LED Load.

14 Thermal Performance

14.1 Thermal Performance Closed Frame



Figure 31 – Test Set-up Picture Thermal Inside Enclosure 50 °C - Closed Frame.

Unit in closed frame was placed inside an enclosure to prevent airflow that might affect the thermal measurements. Ambient temperature inside enclosure is around 50 °C. Temperature was measured using type T thermocouple after 3 hour soak time. A 36 V LED panel load is used at full-load.

| No. | Components | Temperature (°C) |
|-----|-----------------------|------------------|
| | | 100 VAC |
| 1 | Ambient Temperature | 52 |
| 2 | D4 – Output Diode | 87.9 |
| 3 | BR1 – Bridge Diode | 78.9 |
| 4 | D5 – Boost Diode | 91.8 |
| 5 | U2 – HiperPFS-4 | 98.8 |
| 6 | U4 – LYTSwitch-6 | 91.1 |
| 7 | T2 – EE25 | 101.3 |
| 8 | T3 – PQ2020 | 98.2 |
| 9 | C8 – Output Capacitor | 75.3 |
| 10 | C13 – Bulk Capacitor | 67.7 |

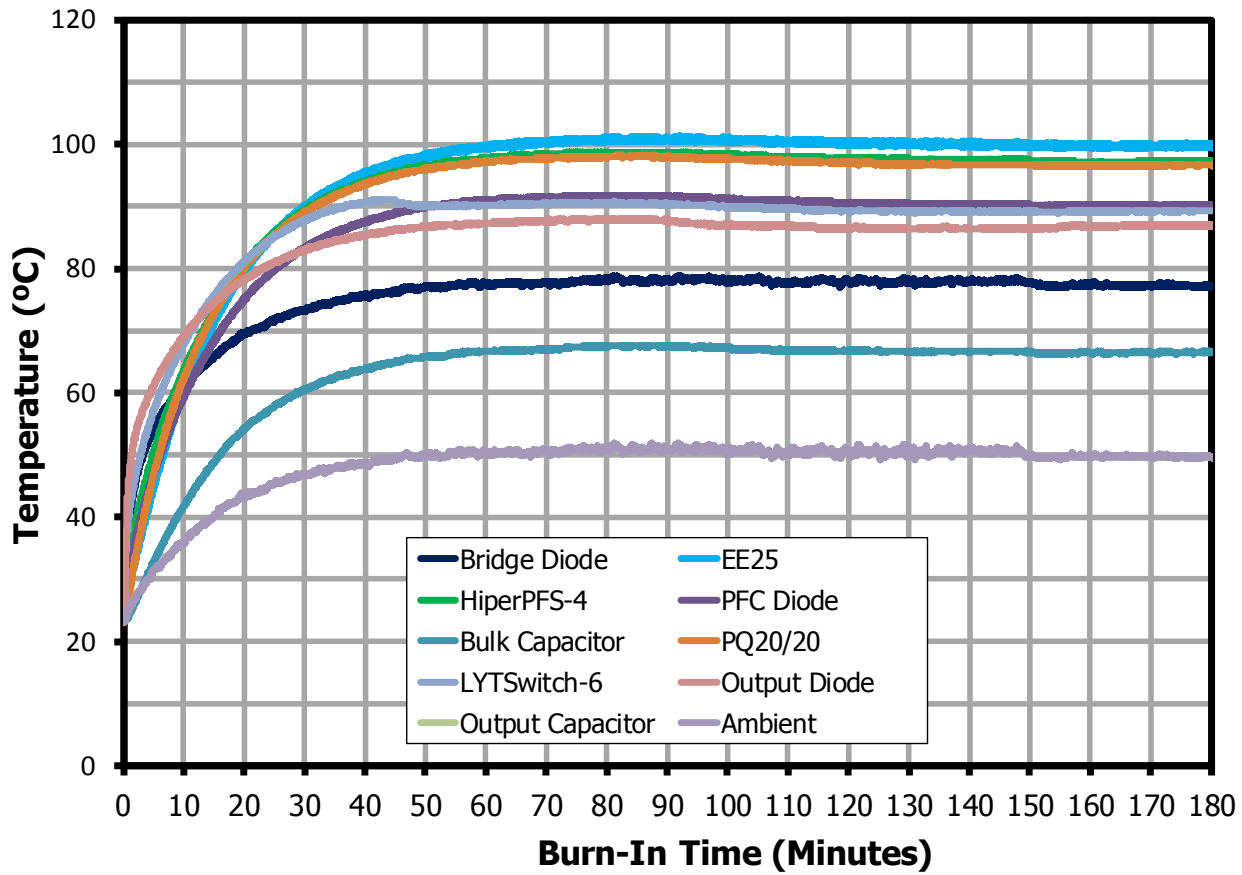


Figure 32 – Thermal Measurements at 25 °C Ambient - Closed Frame 50 °C Ambient.

15 Waveforms

15.1 *Input Voltage and Input Current at 36 V LED Load Panel*

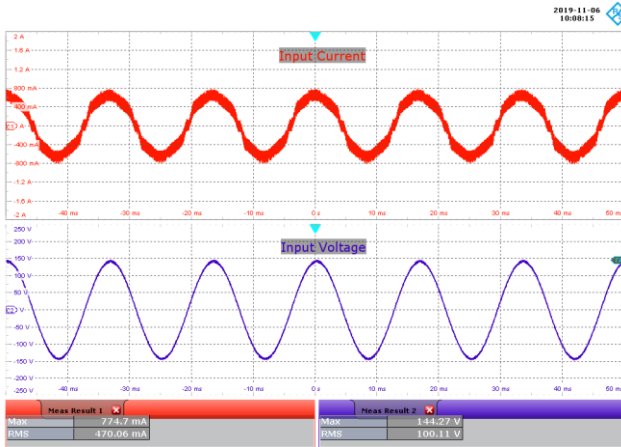


Figure 33 – 100 VAC, 36 V LED Load Panel.
Upper: I_{IN} , 400 mA / div.
Lower: V_{IN} , 100 V / div., 10 ms / div.

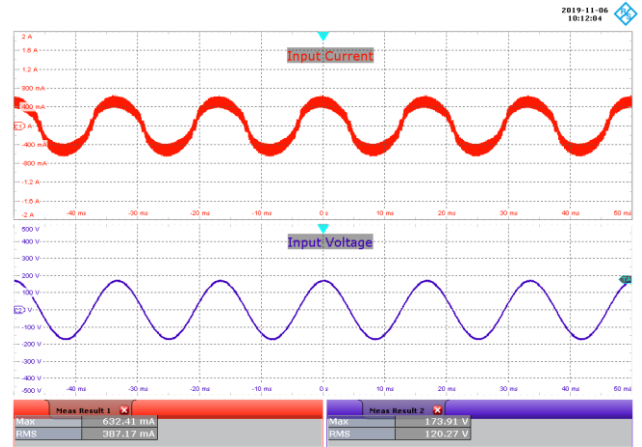


Figure 34 – 120 VAC, 36 V LED Load Panel.
Upper: I_{IN} , 400 mA / div.
Lower: V_{IN} , 100 V / div., 10 ms / div.

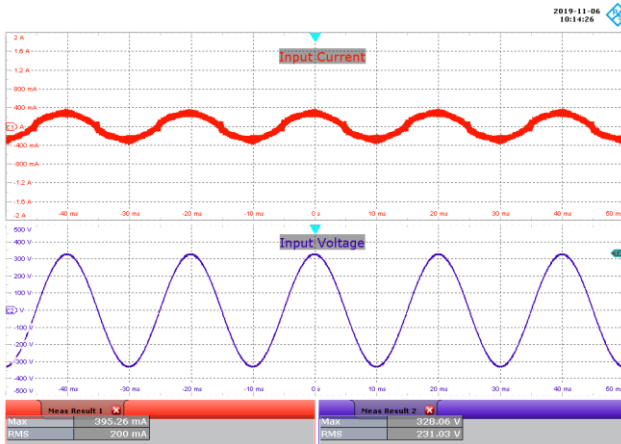


Figure 35 – 230 VAC, 36 V LED Load Panel.
Upper: I_{IN} , 400 mA / div.
Lower: V_{IN} , 100 V / div., 10 ms / div.

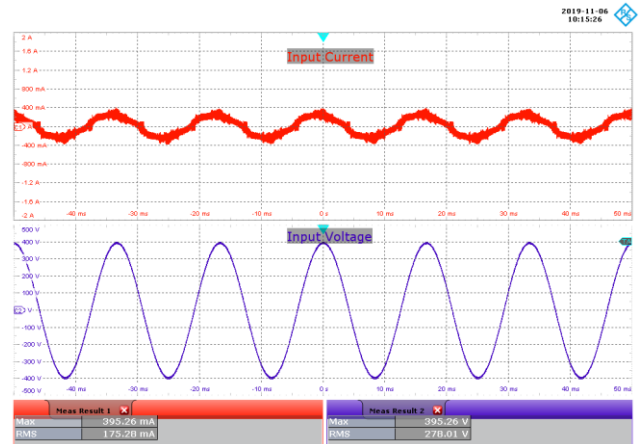


Figure 36 – 277 VAC, 36 V LED Load Panel.
Upper: I_{IN} , 400 mA / div.
Lower: V_{IN} , 100 V / div., 10 ms / div.

15.2 **Start-up Profile at 36 V LED Load Panel**

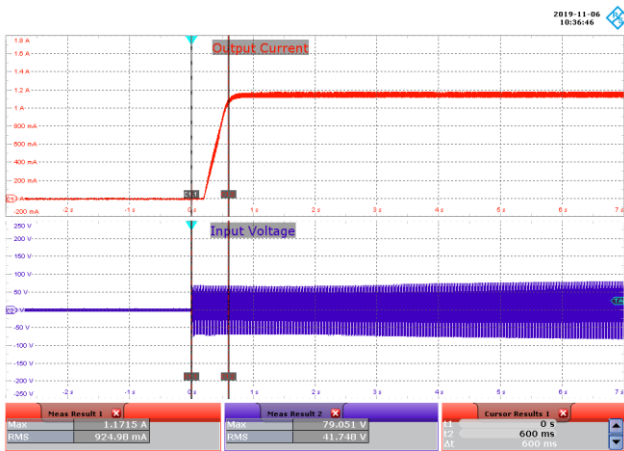


Figure 37 – 100 VAC, 36 V LED, Output Rise.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 50 V / div., 1 s / div.
 Turn-on Time: 600 ms.

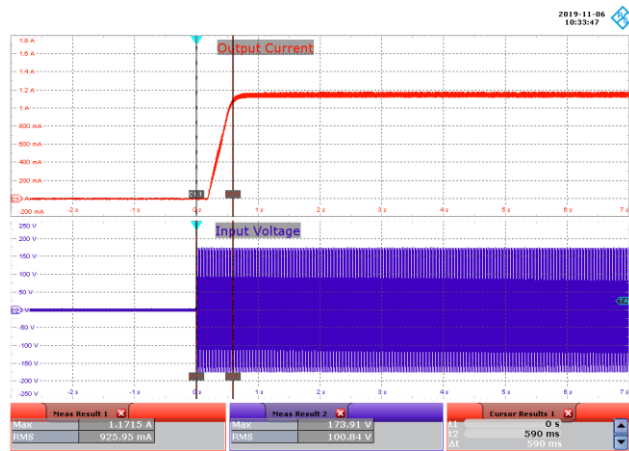


Figure 38 – 120 VAC, 36 V LED, Output Rise.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 50 V / div., 1 s / div.
 Turn-on Time: 590 ms.

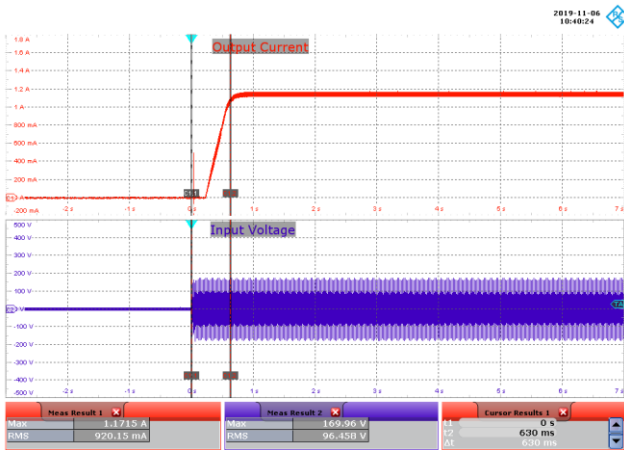


Figure 39 – 230 VAC, 36 V LED, Output Rise.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 1 s / div.
 Turn-on Time: 630 ms.

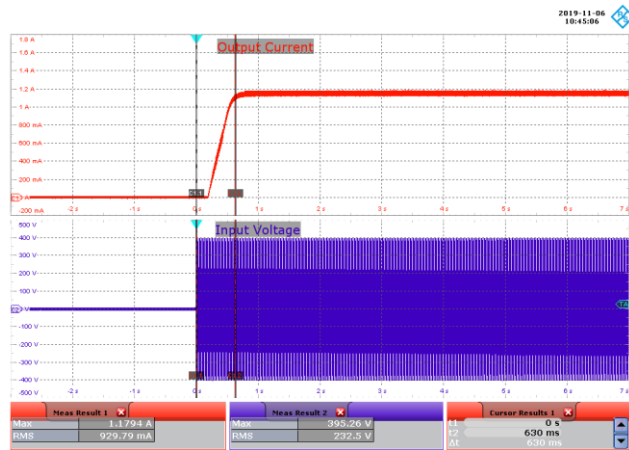


Figure 40 – 277 VAC, 36 V LED, Output Rise.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 1 s / div.
 Turn-on Time: 630 ms.

15.3 **Output Current Fall at 36 V LED Load Panel**

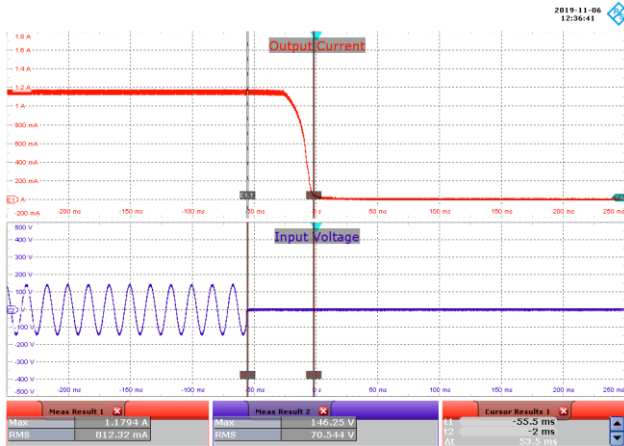


Figure 41 – 100 VAC, 36 V LED, Output Fall.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 50 ms / div.
 Hold-up Time: 53.5 ms.

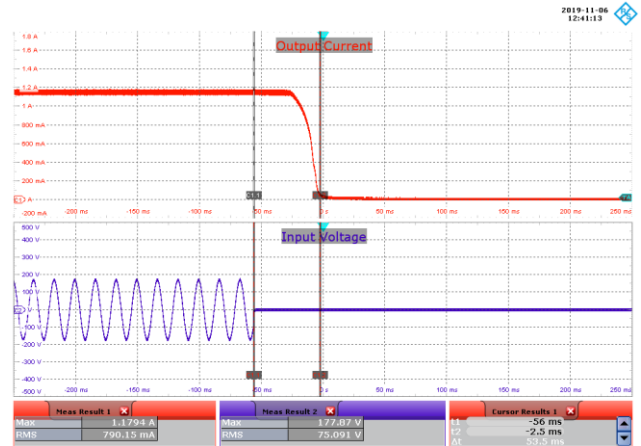


Figure 42 – 120 VAC, 36 V LED, Output Fall.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 50 ms / div.
 Hold-up Time: 53.5 ms.

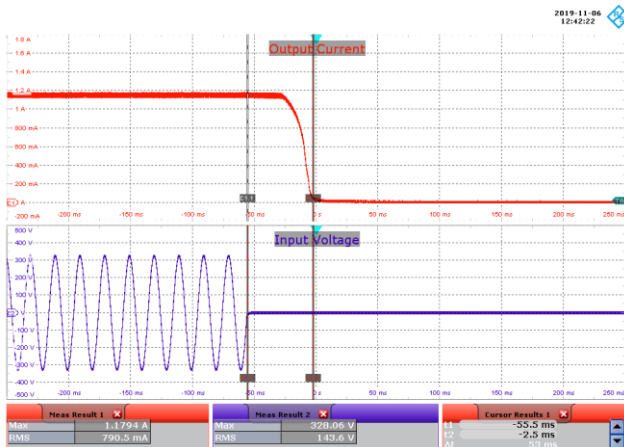


Figure 43 – 230 VAC, 36 V LED, Output Fall.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 50 ms / div.
 Hold-up Time: 53 ms.

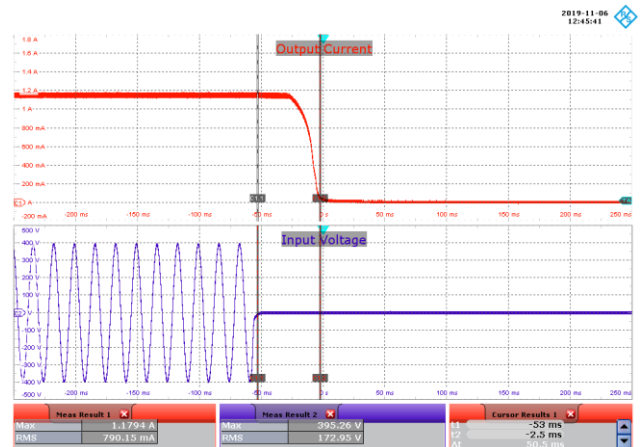


Figure 44 – 277 VAC, 36 V LED, Output Fall.
 Upper: I_{OUT} , 200 mA / div.
 Lower: V_{IN} , 100 V / div., 50 ms / div.
 Hold-up Time: 50.5 ms.

15.4 **AC Cycling Test at 36 V**

No voltage and current overshoots observed during AC power cycling.

15.4.1 2 s OFF, 2 s ON

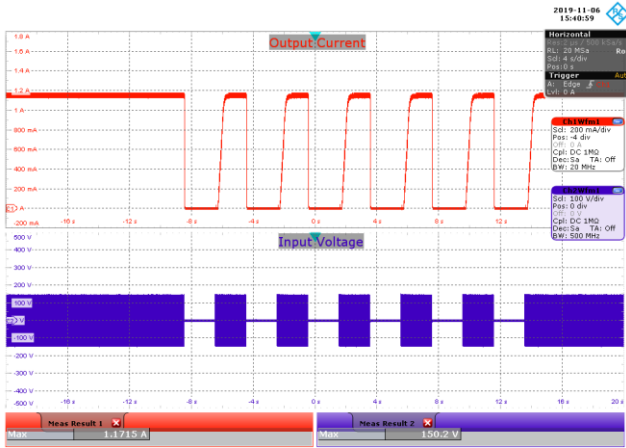


Figure 45 – 100 VAC, 36 V LED.
Upper: I_{OUT} , 200 mA / div.
Lower: V_{IN} , 100 V / div., 4 s / div.

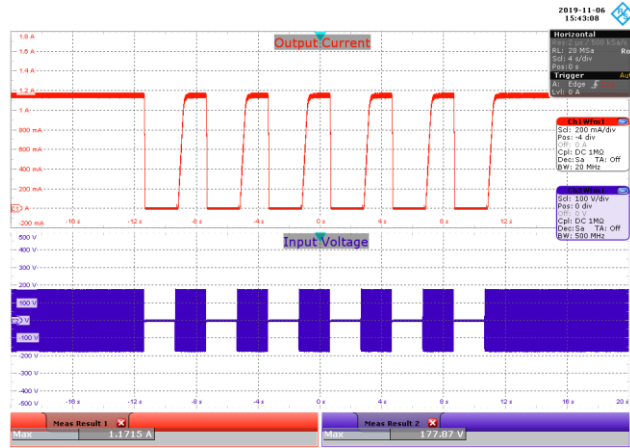


Figure 46 – 120 VAC, 36 V LED.
Upper: I_{OUT} , 200 mA / div.
Lower: V_{IN} , 100 V / div., 4 s / div.

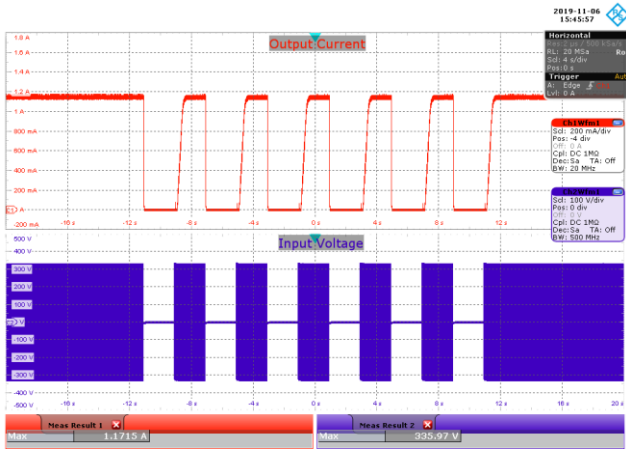


Figure 47 – 230 VAC, 36 V LED.
Upper: I_{OUT} , 200 mA / div.
Lower: V_{IN} , 100 V / div., 4 s / div.

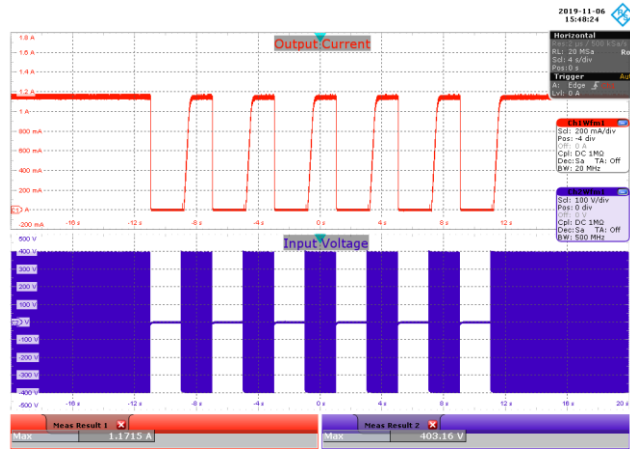


Figure 48 – 277 VAC, 36 V LED.
Upper: I_{OUT} , 200 mA / div.
Lower: V_{IN} , 100 V / div., 4 s / div.

15.5 **PFS7623C (U2) Drain Voltage and Current at Normal Operation**

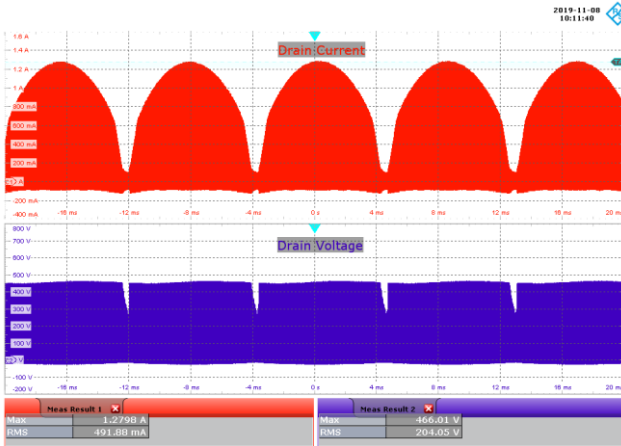


Figure 49 – 100 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 200 mA / div.
Lower: V_{DRAIN} , 100 V / div., 4 ms / div.

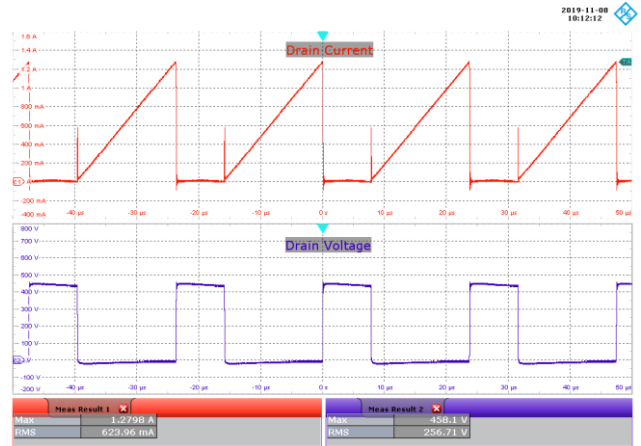


Figure 50 – 100 VAC, 36 V LED Load.
Upper: I_{DRAIN} , 200 mA / div.
Lower: V_{DRAIN} , 100 V / div., 10 μ s / div.

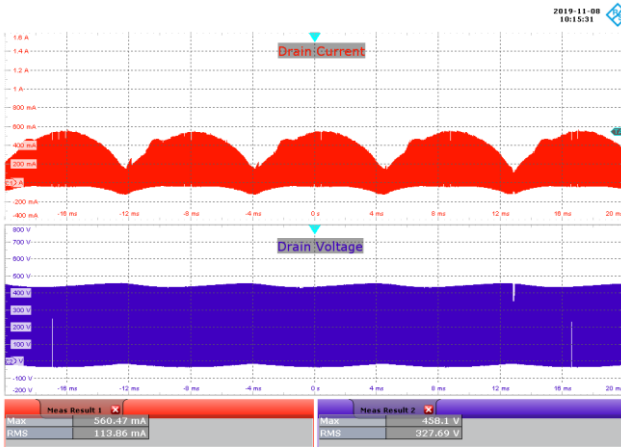


Figure 51 – 277 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 200 mA / div.
Lower: V_{DRAIN} , 100 V / div., 4 ms / div.

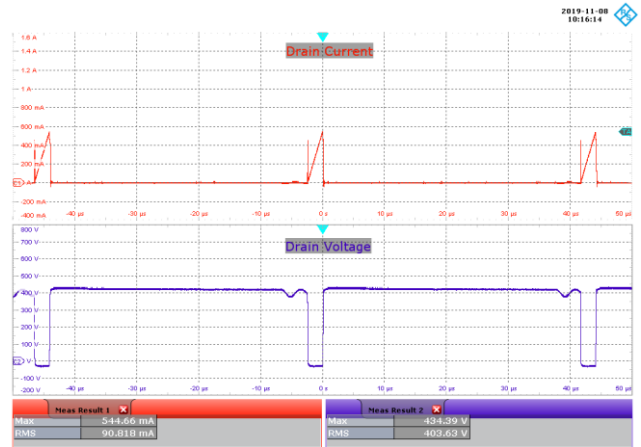


Figure 52 – 277 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 200 mA / div.
Lower: V_{DRAIN} , 100 V / div., 10 μ s / div.

15.6 **PFS7623C (U2) Drain Voltage and Current at Start-up**

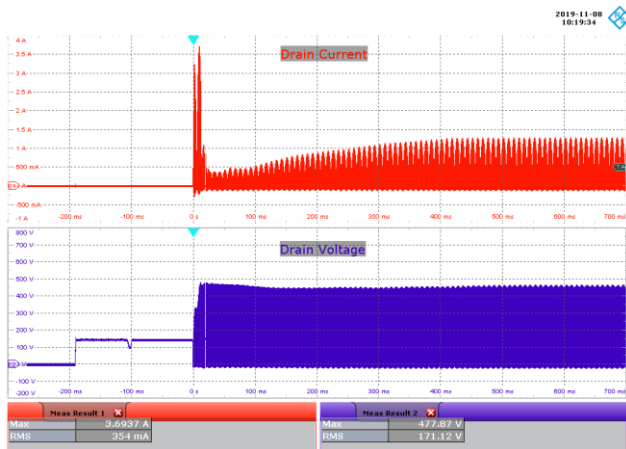


Figure 53 – 100 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 500 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 100 ms / div.

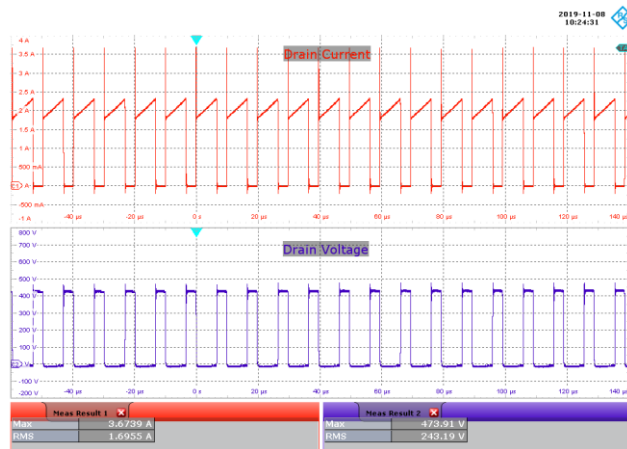


Figure 54 – 100 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 500 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 20 μ s / div.

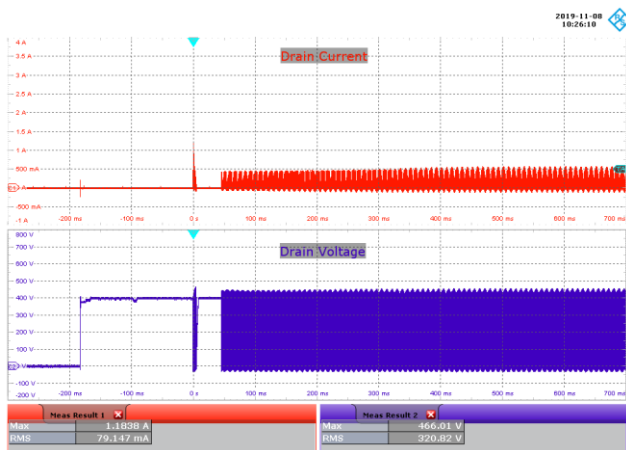


Figure 55 – 277 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 500 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 100 ms / div.

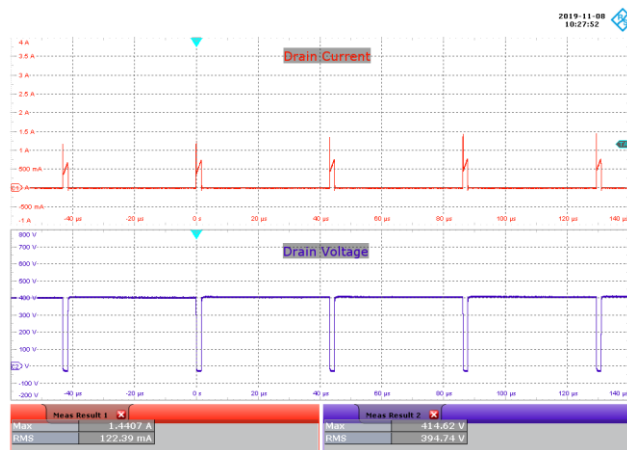


Figure 56 – 277 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 500 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 20 μ s / div.

15.7 **LYTSwitch-6 (U4) Drain Voltage and Current at Normal Operation**

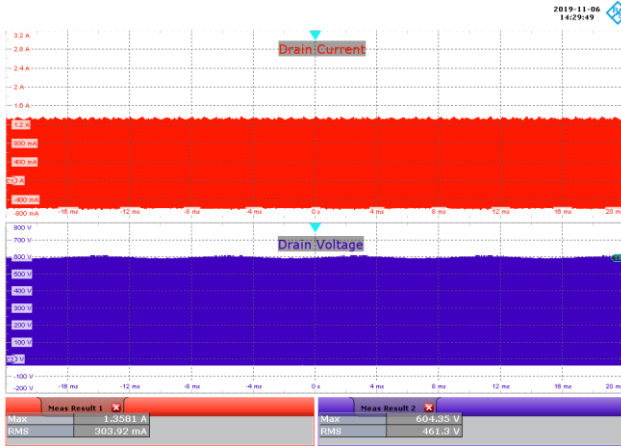


Figure 57 – 120 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 4 ms / div.

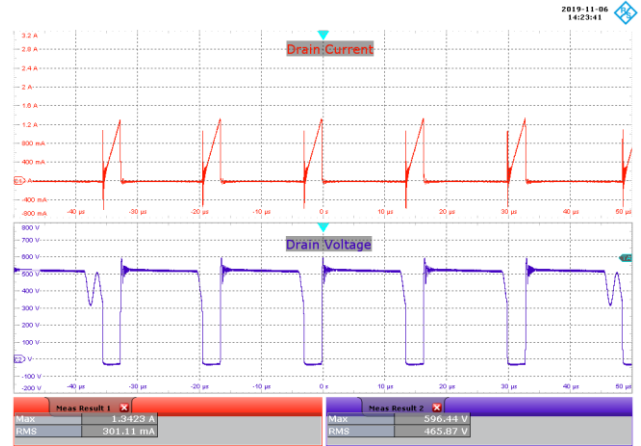


Figure 58 – 120 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 10 μ s / div.

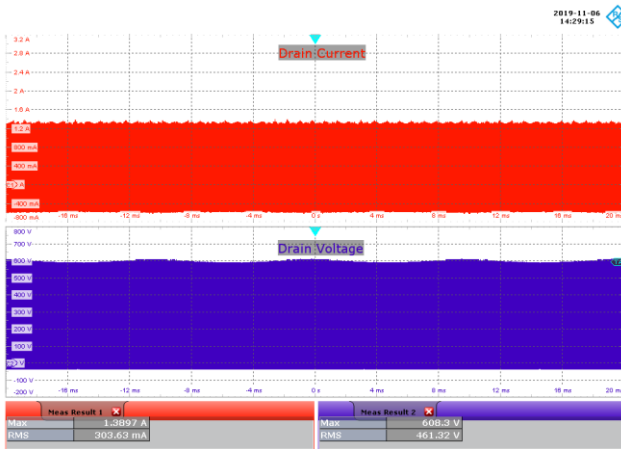


Figure 59 – 230 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 4 ms / div.

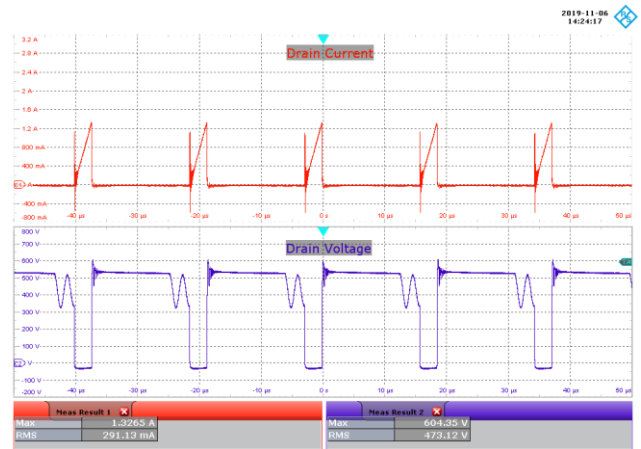


Figure 60 – 230 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 10 μ s / div.

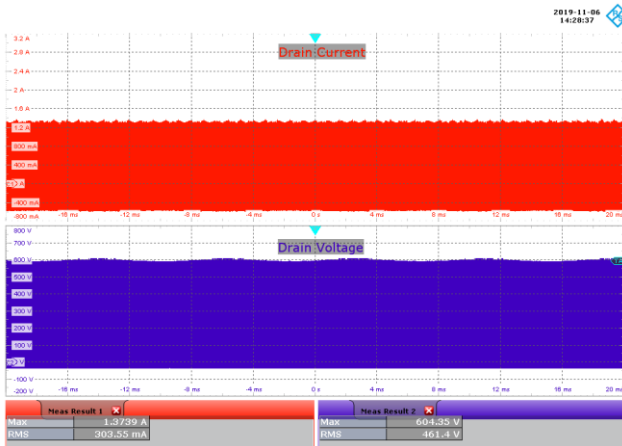


Figure 61 – 277 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 4 ms / div.

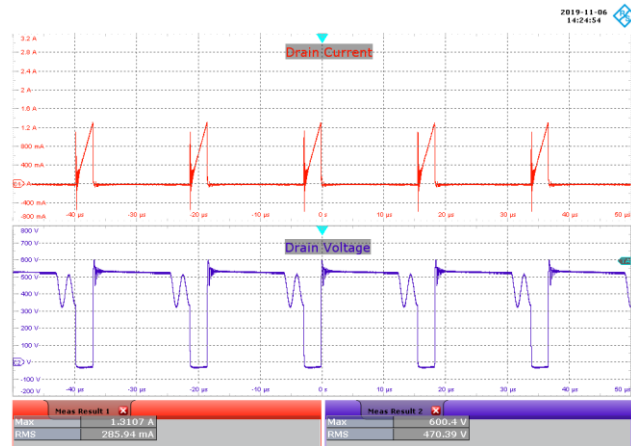


Figure 62 – 277 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 10 μ s / div.

15.8 *LYTswitch-6 (U4) Drain Voltage and Current at Start-up*



Figure 63 – 100 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 200 ms / div.

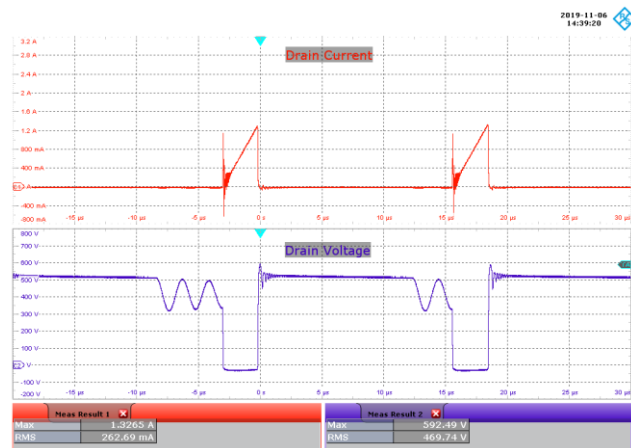


Figure 64 – 100 VAC, 36 V LED Load Panel.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 5 μ s / div.

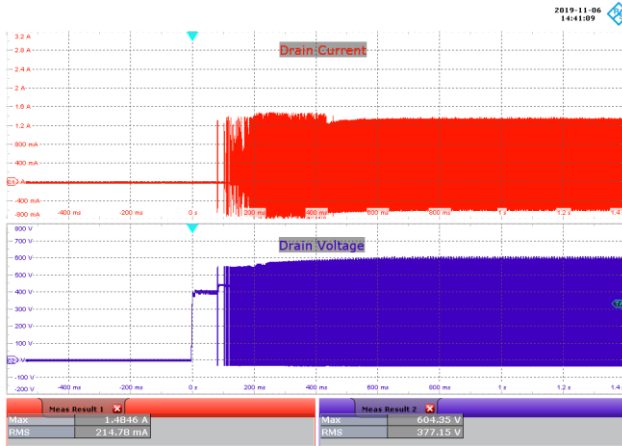


Figure 65 – 277 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 400 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 200 ms / div.

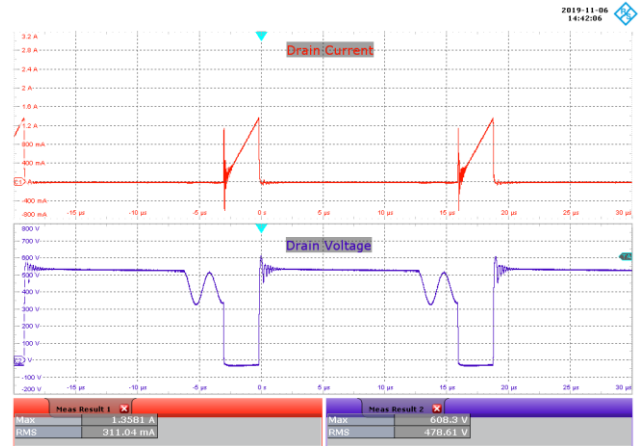


Figure 66 – 277 VAC, 36 V LED Load Panel.
 Upper: I_{DRAIN} , 400 mA / div.
 Lower: V_{DRAIN} , 100 V / div., 5 μ s / div.

15.9 **LYTswitch-6 (U4) Drain Voltage and Current during Output Short-Circuit**

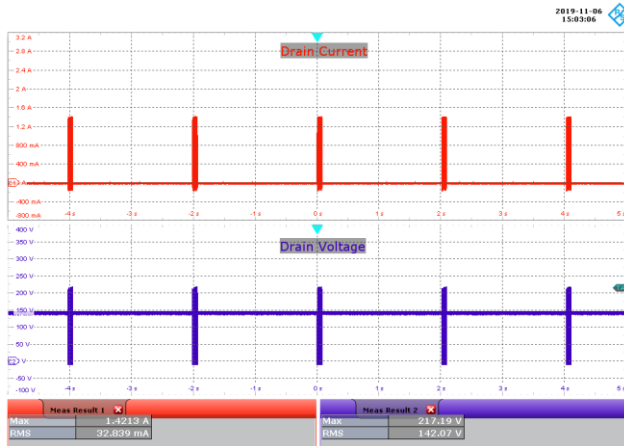


Figure 67 – 100 VAC, Output Shorted.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 50 V / div., 1 s / div.

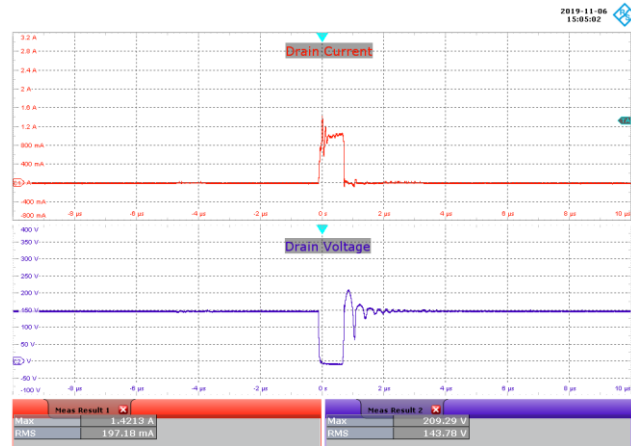


Figure 68 – 100 VAC, Output Shorted.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 50 V / div., 2 μs / div.

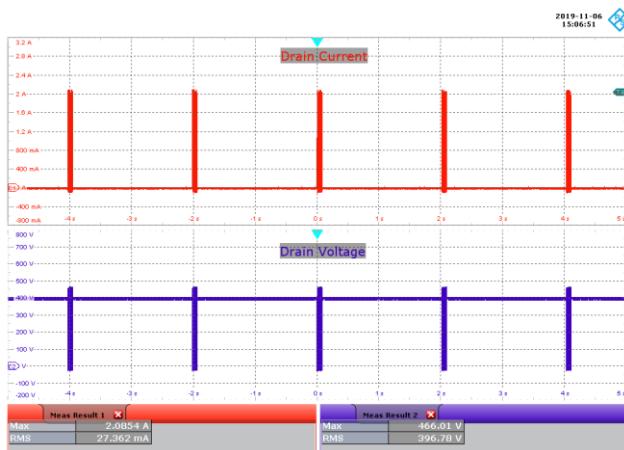


Figure 69 – 277 VAC, Output Shorted.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 1 s / div.

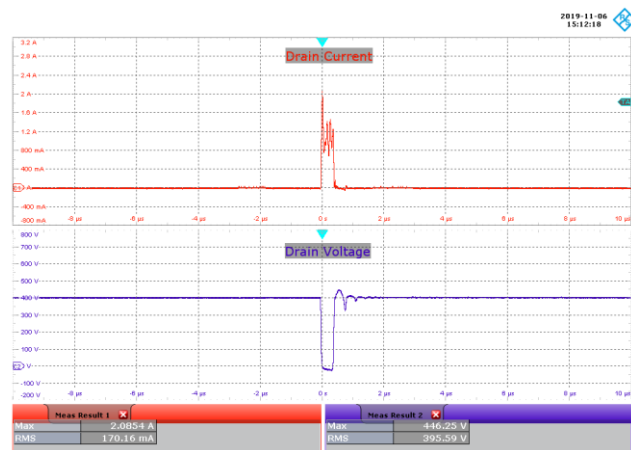


Figure 70 – 277 VAC, Output Shorted.
Upper: I_{DRAIN} , 400 mA / div.
Lower: V_{DRAIN} , 100 V / div., 2 μs / div.

15.10 **Input Power during Output Short-Circuit**

| Input Power at Output Short | | |
|-----------------------------|----------------|-------|
| VAC (V _{RMS}) | Frequency (Hz) | P (W) |
| 100 | 60 | 0.070 |
| 120 | 60 | 0.084 |
| 230 | 50 | 0.168 |
| 277 | 60 | 0.212 |

15.11 **Output Ripple Current at 36 V LED Load Panel**

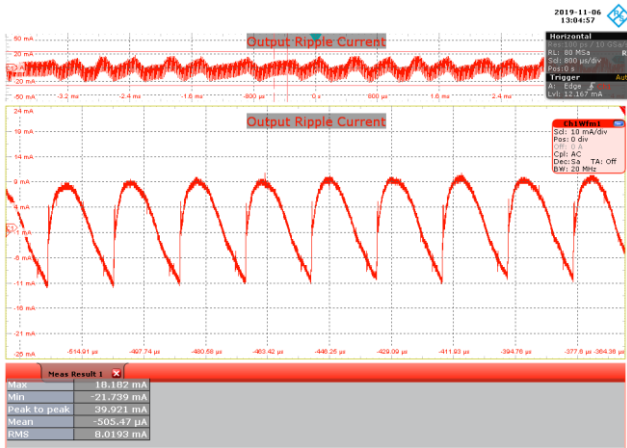


Figure 71 – 100 VAC, 50 Hz, 36 V LED Load Panel.
Upper: I_{OUT} , 10 mA / div., 800 μ s / div.

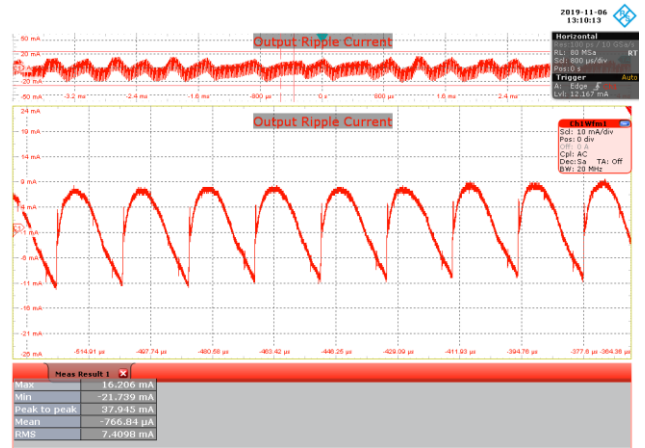


Figure 72 – 120 VAC, 60 Hz, 36 V LED Load Panel.
Upper: I_{OUT} , 10 mA / div., 800 μ s / div.

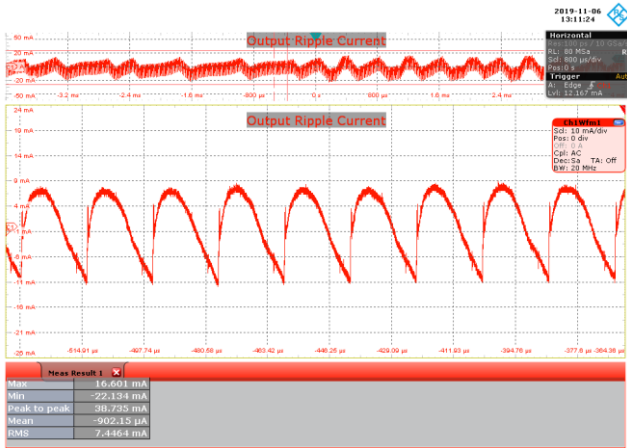


Figure 73 – 230 VAC, 50 Hz, 36 V LED Load Panel.
Upper: I_{OUT} , 10 mA / div., 800 μ s / div.

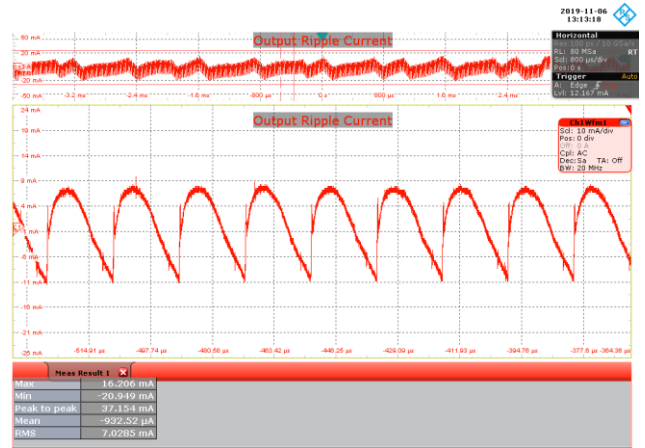


Figure 74 – 277 VAC, 60 Hz, 36 V LED Load Panel.
Upper: I_{OUT} , 10 mA / div., 800 μ s / div.

| V_{IN} (VAC) | I_{PK-PK} (mA) | I_{MEAN} (mA) | % Ripple | | % Flicker | |
|-------------------|---------------------|--------------------|-------------------------------------|--|-----------|--|
| | | | $100 \times (I_{RP-P}) / (I_{OUT})$ | $100 \times (I_{RP-P}) / (2 \times I_{OUT})$ | | |
| 100 | 39.92 | 1150 | 3.47 | 1.74 | | |
| 120 | 37.95 | | 3.30 | 1.65 | | |
| 230 | 38.74 | | 3.37 | 1.68 | | |
| 277 | 37.15 | | 3.23 | 1.62 | | |



16 Conducted EMI

16.1 Test Set-up

The LED panel metal heat sink is connected to earth (yellow-green wire). Unit casing with input ground wire connection is placed on top of LED panel heat sink. The data were measured after 15 minutes soak time. See below set-up picture.

16.2 Equipment and Load Used

1. Rohde and Schwarz ENV216 two line V-network.
2. Rohde and Schwarz ESRP EMI test receiver.
3. Hioki 3322 power hitester.
4. Chroma measurement test fixture.
5. 36 V LED Load Panel with input voltage set at 120VAC and 230 VAC.

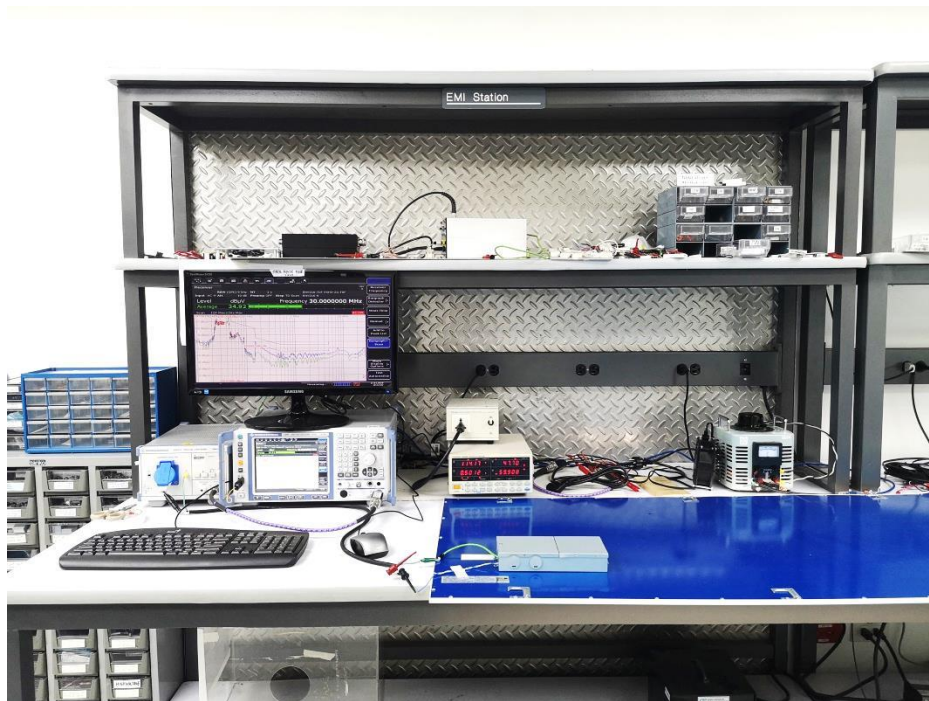


Figure 75 – Conducted EMI Test Set-up.

16.2.1 EMI Test Results

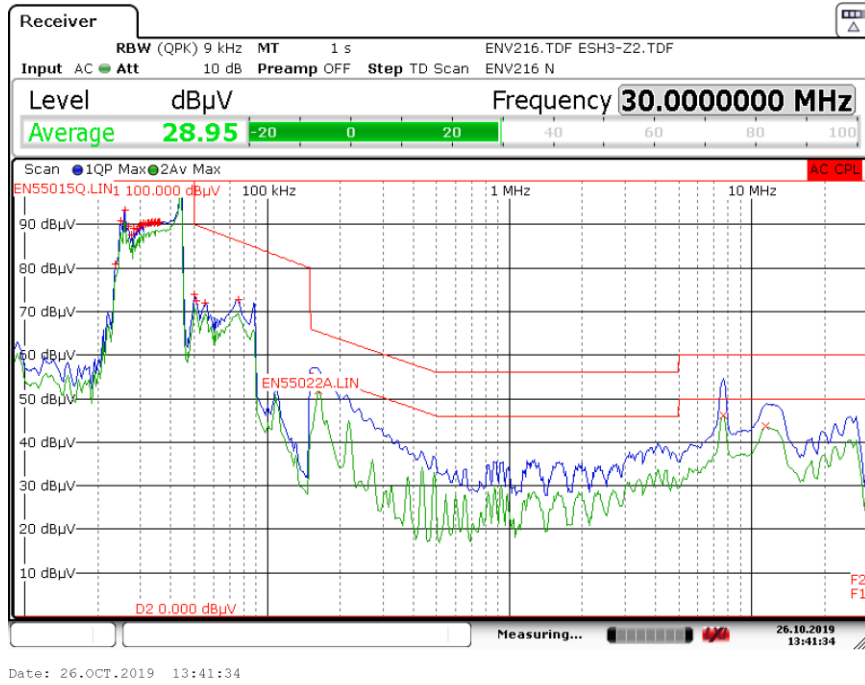


Figure 76 – Conducted EMI QP Scan at 36 V LED Load Panel, 115 VAC, 60 Hz, and EN55015 B Limits.

| Trace1: EN55015Q.LIN | | Trace2: EN55022A.LIN | |
|----------------------|--------------|----------------------|------------|
| Trace/Detector | Frequency | Level dBµV | DeltaLimit |
| 2 Average | 163.5000 kHz | 51.74 | -3.54 dB |
| 2 Average | 7.6453 MHz | 46.27 | -3.73 dB |
| 2 Average | 11.4545 MHz | 43.56 | -6.44 dB |
| 1 Quasi Peak | 44.2000 kHz | 101.61 N | -8.39 dB |
| 1 Quasi Peak | 76.1500 kHz | 72.82 N | -13.35 dB |
| 1 Quasi Peak | 25.8000 kHz | 93.39 N | -16.61 dB |
| 1 Quasi Peak | 55.3000 kHz | 72.08 L1 | -17.00 dB |
| 1 Quasi Peak | 50.9500 kHz | 72.55 N | -17.28 dB |
| 1 Quasi Peak | 24.7500 kHz | 90.93 N | -19.07 dB |
| 1 Quasi Peak | 33.6500 kHz | 90.64 N | -19.36 dB |
| 1 Quasi Peak | 34.6500 kHz | 90.62 N | -19.38 dB |
| 1 Quasi Peak | 36.0000 kHz | 90.53 N | -19.47 dB |
| 1 Quasi Peak | 35.5500 kHz | 90.46 N | -19.54 dB |
| 1 Quasi Peak | 35.1000 kHz | 90.39 N | -19.61 dB |

Insert Frequency Delete Frequency Sort by Frequency
 Symbols OFF ON Peak List Export Decim Sep

Figure 77 – Conducted EMI Data at 115 VAC, 36 V LED Load Panel.



16.2.2 EMI Test Results



Figure 78 – Conducted EMI QP Scan at 36 V LED Load Panel, 230 VAC, 60 Hz, and EN55015 B Limits.

| Trace1: EN55015Q.LIN | | Trace2: EN55022A.LIN | |
|----------------------|--------------|----------------------|------------|
| Trace/Detector | Frequency | Level dBµV | DeltaLimit |
| 2 Average | 7.6475 MHz | 45.47 L1 | -4.53 dB |
| 2 Average | 13.2613 MHz | 45.31 L1 | -4.69 dB |
| 1 Quasi Peak | 65.1500 kHz | 82.24 N | -5.35 dB |
| 1 Quasi Peak | 7.6318 MHz | 54.13 N | -5.87 dB |
| 2 Average | 165.7500 kHz | 48.65 N | -6.52 dB |
| 1 Quasi Peak | 13.5313 MHz | 52.11 L1 | -7.89 dB |
| 1 Quasi Peak | 150.0000 kHz | 57.74 L1 | -8.26 dB |
| 2 Average | 27.1438 MHz | 41.17 L1 | -8.83 dB |
| 2 Average | 222.0000 kHz | 40.64 N | -12.10 dB |
| 1 Quasi Peak | 27.3395 MHz | 46.65 N | -13.35 dB |
| 2 Average | 496.5000 kHz | 31.97 L1 | -14.09 dB |
| 2 Average | 442.5000 kHz | 30.85 N | -16.16 dB |
| 2 Average | 555.0000 kHz | 28.02 L1 | -17.98 dB |
| 2 Average | 890.2500 kHz | 27.17 L1 | -18.83 dB |

Buttons: Insert Frequency, Delete Frequency, Sort by Frequency, Symbols OFF ON, Peak List Export, Decim Sep

Figure 79 – Conducted EMI Data at 230 VAC, 36 V LED Load Panel.

17 Line Surge

The unit was subjected to ± 2500 V, 100 kHz ring wave and ± 1000 V differential surge with 10 strikes at each condition. A test failure was defined as a non-recoverable interruption of output requiring repair or recycling of input voltage.

17.1 Differential Surge Test Results

| Surge Level (V) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Line Impedance (Ω) | Test Result (Pass/Fail) |
|-----------------|---------------------|--------------------|---------------------|-----------------------------|-------------------------|
| +1000 | 115 | L to N | 0 | 2 | Pass |
| -1000 | 115 | L to N | 0 | 2 | Pass |
| +1000 | 115 | L to N | 90 | 2 | Pass |
| -1000 | 115 | L to N | 90 | 2 | Pass |
| +1000 | 115 | L to N | 270 | 2 | Pass |
| -1000 | 115 | L to N | 270 | 2 | Pass |
| +1000 | 230 | L to N | 0 | 2 | Pass |
| -1000 | 230 | L to N | 0 | 2 | Pass |
| +1000 | 230 | L to N | 90 | 2 | Pass |
| -1000 | 230 | L to N | 90 | 2 | Pass |
| +1000 | 230 | L to N | 270 | 2 | Pass |
| -1000 | 230 | L to N | 270 | 2 | Pass |

17.2 Ring Wave Surge Test Results

| Surge Level (V) | Input Voltage (VAC) | Injection Location | Injection Phase (°) | Line Impedance (Ω) | Test Result (Pass/Fail) |
|-----------------|---------------------|--------------------|---------------------|-----------------------------|-------------------------|
| +2500 | 115 | L to N | 0 | 12 | Pass |
| -2500 | 115 | L to N | 0 | 12 | Pass |
| +2500 | 115 | L to N | 90 | 12 | Pass |
| -2500 | 115 | L to N | 90 | 12 | Pass |
| +2500 | 115 | L to N | 270 | 12 | Pass |
| -2500 | 115 | L to N | 270 | 12 | Pass |
| +2500 | 230 | L to N | 0 | 12 | Pass |
| -2500 | 230 | L to N | 0 | 12 | Pass |
| +2500 | 230 | L to N | 90 | 12 | Pass |
| -2500 | 230 | L to N | 90 | 12 | Pass |
| +2500 | 230 | L to N | 270 | 12 | Pass |
| -2500 | 230 | L to N | 270 | 12 | Pass |

18 Brown-in/Brown-out Test

No abnormal overheating, current overshoot/undershoot was observed during and after 0.5 V / s and 1 V / s brown in and brown out test.

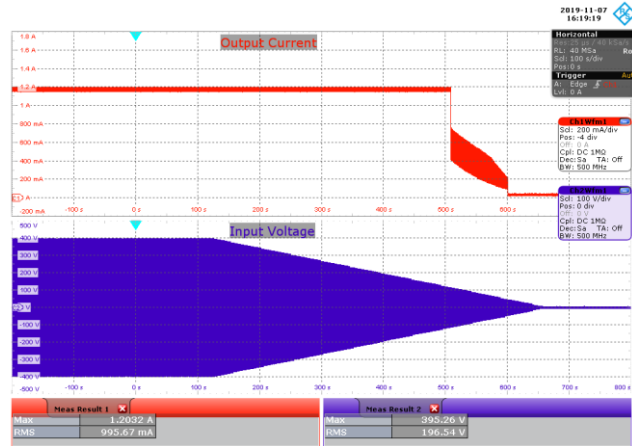
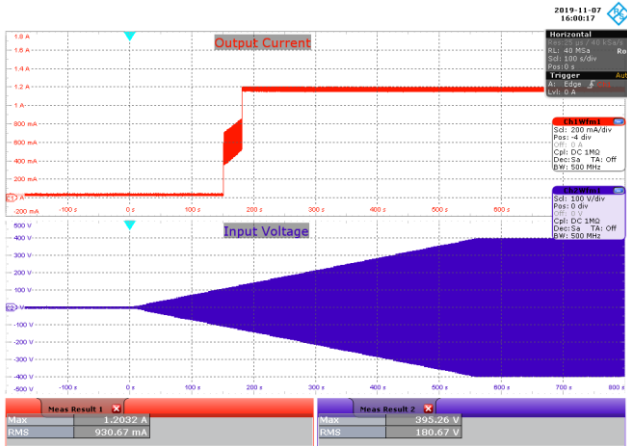


Figure 80 – Brown-in Test at 0.5 V / s.
 Ch1: I_{OUT}, 200 mA / div.
 Ch2: V_{IN}, 100 V / div.
 Time Scale: 100 s / div.

Figure 81 – Brown-out Test at 0.5 V / s
 Ch1: I_{OUT}, 200 mA / div.
 Ch2: V_{IN}, 100 V / div.
 Time Scale: 100 s / div.

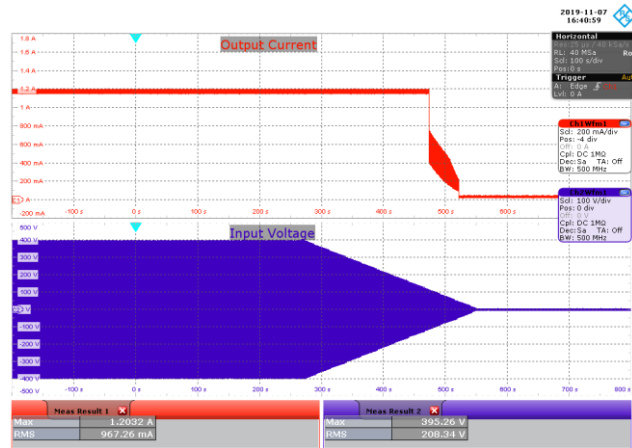
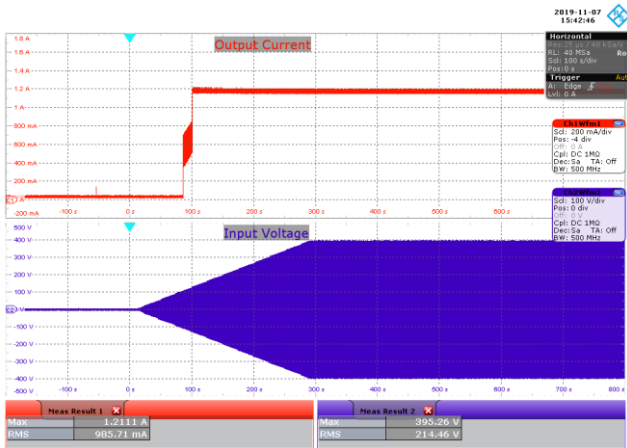


Figure 82 – Brown-in Test at 1 V / s.
 Ch1: I_{OUT}, 200 mA / div.
 Ch2: V_{IN}, 100 V / div.
 Time Scale: 100 s / div.

Figure 83 – Brown-out Test at 1 V / s.
 Ch1: I_{OUT}, 200 mA / div.
 Ch2: V_{IN}, 100 V / div.
 Time Scale: 100 s / div.

19 Revision History

| Date | Author | Revision | Description and Changes | Reviewed |
|-------------|---------------|-----------------|--------------------------------|-----------------|
| 16-Jan-20 | JB & CA | 1.0 | Initial Release. | Apps & Mktg |
| | | | | |
| | | | | |



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